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Effect of a static external magnetic perturbation on resistive mode stability in tokamaks

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The influence of a general static external magnetic perturbation on the stability of resistive modes in a tokamak plasma is examined. There are three main parts to this investigation. First, the vacuum perturbation is expanded as a set of well-behaved toroidal ring functions, and is, thereafter, specified by the coefficients of this expansion. Second, a dispersion relation is derived for resistive plasma instabilities in the presence of a general external perturbation, and finally, this dispersion relation is solved for the amplitudes of the tearing and twisting modes driven in the plasma by a specific perturbation. It is found that the amplitudes of driven tearing and twisting modes are negligible until a certain critical perturbation strength is exceeded. Only tearing modes are driven in low-β plasmas with $\epsilon\beta_p \ll 1$. However, twisting modes may also be driven if $\epsilon\beta_p \gtrsim 1$. For error-field perturbations made up of a large number of different poloidal and toroidal harmonics the critical strength to drive locked modes has a "staircase" variation with edge-q, characterized by strong discontinuities as coupled rational surfaces enter or leave the plasma. For single harmonic perturbations, the variation with edge-q is far smoother. Both types of behavior have been observed experimentally. The critical perturbation strength is found to decrease strongly close to an ideal external kink stability boundary. This is also in agreement with experimental observations.

I. INTRODUCTION

Recent experimental and theoretical results have lead to a greatly increased understanding of the influence of a static external magnetic perturbation on resistive mode stability in a tokamak plasma.[1-10] It is found that plasma rotation inhibits externally driven magnetic reconnection until a certain critical perturbation amplitude is exceeded. The critical amplitude decreases strongly with increasing machine dimensions because of the relatively slow intrinsic plasma rotation in large devices,[9] but can be artificially increased by spinning the plasma with unbalanced neutral beam injection (NBI).[5] The critical amplitude is sufficiently small in the largest present-day devices to allow field errors, due, for instance, to misalignment of poloidal field coils, to drive magnetic reconnection in otherwise stable plasmas.[1,10] This effect can significantly reduce the disruption-free operating space at low plasma densities, and may, therefore, need to be taken into account in the ongoing International Tokamak Experimental Reactor (ITER) Engineering Design Activity.[11]

Existing theories describing the interaction of a static external magnetic perturbation with a rotating tokamak plasma are limited to zero β in slab or cylindrical geometry.[2,6,8,9] We aim to extend the theory of this interaction to both finite β and toroidal geometry. There are, of course, a number of complications. At zero β only tearing parity plasma instabilities need to be taken into account, whereas at finite β, twisting parity modes must also be included in the analysis.[12] Furthermore, in toroidal geometry magnetic perturbations with different poloidal mode numbers are coupled together. As is described in Sec. II, the dispersion relation for externally driven resistive modes in a

plasma possessing N rational surfaces takes the form of two coupled $N \times N$ matrix equations.[12] In Sec. III we use this dispersion relation to investigate the response of intrinsically stable tearing and twisting modes to a generalized external perturbation. In Secs. IV and V, we classify and characterize the external perturbations that are likely to occur in experimental situations, using results from the recently developed T7 code.[13] Our main conclusions are summarized in Sec. VI.

II. THE DISPERSION RELATION FOR EXTERNALLY DRIVEN RESISTIVE INSTABILITIES

A. Asymptotic matching

The analysis of resistive instabilities in a high-temperature tokamak is generally facilitated by dividing the plasma into two regions.[14] In the "outer" region, which comprises most of the plasma, a general instability is governed by the equations of ideal magnetohydrodynamics (MHD), which are equivalent to the requirement of force balance in an incompressible, perfectly conducting fluid.[15] The "inner" region is localized around so-called rational flux surfaces, where the helical pitch of equilibrium magnetic field lines resonates with that of the instability. The ideal MHD equations are, in fact, singular at the rational surfaces. The physical solution is obtained by asymptotically matching the outer solution across a set of thin layers centered on the rational surfaces. In these layers, nonideal effects such as plasma resistivity, inertia, viscosity, and compressibility are important.

B. The dispersion relation

Suppose that there are N rational surfaces in the plasma resonant with toroidal mode number n. Let $r_1 < r_2 < \cdots r_N$ be the minor radii of these surfaces, and $m_1, m_2, \cdots m_N$ the

resonant poloidal mode numbers. There are, in general, $2N$ independent resistive modes. It is convenient to resolve a general mode into components of N basis tearing modes and N basis twisting modes. The jth basis tearing mode ($1 \leq j \leq N$) is defined to have unit tearing amplitude and zero twisting amplitude at rational surface j, with zero tearing or twisting amplitude at any other surface. Likewise, the jth basis twisting mode has unit twisting amplitude and zero tearing amplitude at surface j, with zero tearing or twisting amplitude at any other surface. Here, the tearing amplitude at surface j is basically the even (with respect to the rational surface) component of the perturbed normal resonant magnetic field, whereas the twisting amplitude is the odd component (see the Appendix for more exact definitions).

The most general dispersion relation for coupled tearing and twisting modes in the presence of an external perturbation takes the form (see the Appendix)[12,16]

$$[\boldsymbol{\Delta}^+(\omega) - \mathbf{E}^+]\boldsymbol{\Psi}^+ - \mathbf{H}\boldsymbol{\Psi}^- = \mathbf{C}^+, \tag{1a}$$

$$[\boldsymbol{\Delta}^-(\omega) - \mathbf{E}^-]\boldsymbol{\Psi}^- - \mathbf{H}^\dagger\boldsymbol{\Psi}^+ = \mathbf{C}^-, \tag{1b}$$

where $\mathbf{E}^\pm$ is an $N \times N$ real symmetric matrix, $\mathbf{H}$ is an $N \times N$ real matrix and $\mathbf{H}^\dagger$ is its transpose, $\boldsymbol{\Delta}^\pm(\omega)$ is the $N \times N$ complex diagonal matrix of the $\Delta_j^\pm(\omega)$ values, $\boldsymbol{\Psi}^\pm$ is the $1 \times N$ complex vector of the $\Psi_j^\pm$ values, and $\mathbf{C}^\pm$ are $1 \times N$ complex vectors, characterizing the external perturbation. Here, $\Delta_j^+(\omega)$ is the tearing parity stability index for the layer at the rational surface j, and $\Delta_j^-(\omega)$ is the corresponding twisting parity stability index [see Eq. (A11) and Sec. II F]. Also, Ψ_j^+ is the tearing amplitude at surface j, and Ψ_j^- is the corresponding twisting amplitude [see Eq. (A10a)]. The tearing amplitude is sometimes termed the "reconnected flux."

The E^+ matrix determines the intrinsic stability and mutual interaction of basis tearing modes in the plasma. The E^- matrix governs the intrinsic stability of basis twisting modes, and the H matrix specifies the interaction of basis tearing and twisting modes. The evaluation of these matrices in a large aspect ratio, low-β, weakly shaped tokamak equilibrium is discussed in Refs. 12 and 13. The Appendix describes how the components of the $C^\pm$ vectors are calculated for a given external perturbation and plasma equilibrium.

C. The E^+ matrix

Consider a plasma with a monotonic safety factor profile containing no rational surfaces resonant with poloidal mode number $m = 1$. (The restriction to $m > 1$ modes is necessary because the $m = 1$ mode generally requires special treatment in tokamak plasmas.[17]) In such a plasma the diagonal elements of the E^+ matrix take the form

$$E_{jj}^+ = \Delta_j^0 + \mathscr{O}(\epsilon^2), \tag{2}$$

where Δ_j^0 is the standard cylindrical tearing stability index for the m_j/n mode (normalized with respect to r_j). The off-diagonal elements of the E^+ matrix are $\mathscr{O}(\epsilon)$. Coupling of basis tearing modes with resonant poloidal mode numbers differing by unity is affected by the Shafranov shift of flux surfaces, which is driven by toroidicity and the plasma pressure. Coupling of modes with poloidal mode numbers differing by two or three is affected by flux surface ellipticity or

triangularity, respectively.[13] (The "resonant" poloidal mode number of the jth basis tearing or twisting mode is, of course, m_j.)

D. The E^- matrix

For a plasma with a monotonic safety factor profile the E^- matrix is *diagonal* (for the ordering adopted in Refs. 12 and 13), indicating that there is no direct coupling of basis twisting modes possessing different resonant poloidal mode numbers. The jth diagonal element can be written[12] as

$$E_{jj}^- = -\Delta_j^c + e_j m_j(\alpha_j)^2, \tag{3}$$

where Δ_j^c is a stabilizing term emanating from the layer at rational surface j, and

$$\alpha_j = -\left(\frac{2R_0\mu_0 p' q^2}{B_0^2}\right)_{r_j} \tag{4}$$

is a measure of the local pressure gradient at surface j. Here, R_0 is the major radius of the plasma, B_0 is the vacuum magnetic field strength on the magnetic axis, r is the minor radius of flux surfaces, $p(r)$ is the equilibrium pressure profile, $q(r)$ is the safety factor profile, and the prime denotes d/dr. In Eq. (3), e_j is an $\mathscr{O}(1)$ parameter that can be evaluated using $m_j \pm 1/n$ cylindrical basis functions. In Ref. 12, it is demonstrated that to a good approximation,

$$\Delta_j^c = 2.104\beta_j^{1/2}\left(\frac{\tau_R^{2/3}}{\tau_H^{1/3}\tau_V^{1/3}}\right)_{r_j}, \tag{5}$$

in a typical Ohmically heated tokamak plasma, where compressibility, (anomalous) viscosity, and resistivity are the dominant nonideal effects. In the above, $\tau_H = (R_0/B_0)\sqrt{\mu_0\rho(r)}/ns(r)$ is the hydromagnetic time scale, $\tau_R(r) = \mu_0 r^2/\eta_\parallel(r)$ the resistive time scale, $\tau_V(r) = r^2\rho(r)/\mu_\perp(r)$ the viscous time scale, and $\beta_j = \gamma_s\mu_0 p(r_j)/B_0^2$ is a measure of the stabilizing effect of plasma compressibility at surface j. Here, γ_s is the standard ratio of specific heats, $\rho(r)$ is the plasma mass density, $\eta_\parallel(r)$ is the parallel resistivity, $\mu_\perp(r)$ is the (anomalous) perpendicular viscosity, and $s(r) = rq'/q$ is the magnetic shear.

E. The H matrix

For a plasma with a monotonic safety factor profile, the H matrix is *tridiagonal*, indicating that basis tearing modes can couple to basis twisting modes with the same resonant poloidal mode number and with mode numbers differing by unity, and *vice versa*. The jth diagonal element is written[12] as

$$H_{jj} = -\frac{\pi}{2}\frac{\kappa_j}{s_j} + \mathscr{O}(\epsilon^2), \tag{6}$$

where

$$\kappa_j = \left\{-qr\frac{d}{dr}\left[\frac{1}{r}\frac{d}{dr}\left(\frac{r^2}{q}\right)\right]\right\}_{r_j} + \mathscr{O}(\epsilon^2) \tag{7}$$

is a measure of the local equilibrium current gradient at rational surface j. The element of the H matrix which couples

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the basis tearing mode associated with surface j to the basis twisting mode associated with surface k takes the form[12]

$$H_{jk} = h_{jk} m_j \alpha_k, \tag{8}$$

provided $m_k = m_j \pm 1$. The $\mathscr{O}(1)$ parameter h_{jk} can be evaluated using m_j/n cylindrical basis functions.

F. The layer responses

The responses of the resistive layers at the N rational surfaces in the plasma to tearing and twisting parity perturbations from the outer region are specified by the diagonal matrices $\mathbf{\Delta}^+$ and $\mathbf{\Delta}^-$. The jth diagonal element of $\mathbf{\Delta}^+$ (i.e., Δ_j^+) specifies the response of the jth layer to a tearing parity perturbation, and the jth diagonal element of $\mathbf{\Delta}^-$ (i.e., Δ_j^-) specifies the response to a twisting parity perturbation. It turns out that the responses of resistive layers to external perturbations are *resonant* in nature.[2,18] That is, there is virtually no tearing or twisting amplitude driven in a layer, unless the external tearing or twisting parity perturbation rotates in a certain very narrow band of frequencies. The optimum frequency for externally driven tearing amplitude at surface j is equal to the "natural frequency" of the jth basis tearing mode (i.e., the propagation frequency of the uncoupled, intrinsically unstable jth basis tearing mode). Likewise, the optimum frequency for externally driven twisting amplitude at surface j is equal to the natural frequency of the jth basis twisting mode. In Ref. 12, it is shown that to a good approximation,

$$\Delta_j^\pm(\omega) = -i(\omega - \omega_j^\pm)\tau_j, \tag{9}$$

in a typical Ohmically heated tokamak plasma. Here, ω is the mode rotation frequency [all layer quantities are assumed to vary like $\exp(-i\omega t)$],

$$\tau_j = 2.104 \left(\frac{\tau_H^{1/3} \tau_R^{5/6}}{\tau_V^{1/6}} \right)_{r_j} \tag{10}$$

is the reconnection time scale at surface j, ω_j^+ is the natural frequency for tearing parity modes at this surface, and ω_j^- is the corresponding natural frequency for twisting parity modes. Both natural frequencies are determined by local equilibrium plasma flows. Typically, the natural frequencies of tearing and twisting modes differ by of order the local electron diamagnetic frequency.[12] In addition, sheared rotation and diamagnetic flows in the plasma ensure that the natural frequencies of basis modes associated with different rational surfaces are not the same.

G. The $C^\pm$ vectors

The $C^\pm$ vectors are functions of both the plasma equilibrium and the external perturbation. Typical values are given in Secs. IV and V, but for the moment they are assumed to be arbitrary.

III. EXTERNALLY DRIVEN RESISTIVE INSTABILITIES

A. Introduction

In this section, we aim to characterize the solutions of the dispersion relation (1), as fully as possible, for the case of

an arbitrary *static* external magnetic perturbation interacting with an intrinsically stable plasma. In Sec. III B we examine the simple case, where there is only one rational surface in the plasma. In Sec. III C we describe the more complicated situation, where there are two rational surfaces, and in Sec. III D we briefly examine the case of three (or more) surfaces.

B. Stability of a plasma containing a single rational surface

1. Introduction

Consider the simplest possible situation where there is only a single rational surface in the plasma, radius r_1, resonant with poloidal mode number m_1. In this case, the dispersion relation (1) reduces to

$$\Psi_1^+ = \frac{(\Delta_1^- - E_{11}^-)C_1^+ + H_{11}C_1^-}{(\Delta_1^+ - E_{11}^+)(\Delta_1^- - E_{11}^-) - (H_{11})^2},$$

$$\Psi_1^- = \frac{(\Delta_1^+ - E_{11}^+)C_1^- + H_{11}C_1^+}{(\Delta_1^+ - E_{11}^+)(\Delta_1^- - E_{11}^-) - (H_{11})^2}. \tag{11}$$

Now, $|\omega_1^+ - \omega_1^-|\tau_1 \gg 1$ in a typical high-temperature tokamak plasma,[12,18] where ω_1^+ is the natural frequency of tearing parity modes at the rational surface, ω_1^- is the natural frequency of twisting parity modes, and τ_1 is the reconnection time scale. It follows from Eqs. (9) that Δ_1^+ and Δ_1^- are never small simultaneously, so Eqs. (11) reduce to

$$\Psi_1^+ \simeq \frac{C_1^+}{i\omega_1^+ \tau_1 - E_{11}^+},$$

$$\Psi_1^- \simeq \frac{C_1^-}{i\omega_1^- \tau_1 - E_{11}^-}, \tag{12}$$

assuming that the perturbation is static (i.e., $\omega=0$). It is also assumed that the tearing and twisting modes are both intrinsically stable, so that $E_{11}^+ < 0$ and $E_{11}^- < 0$. It is clear from (12) that the C^+ vector drives tearing parity modes in the plasma, whereas the C^- vector drives twisting parity modes.

2. Electromagnetic and viscous torques

The nonlinear toroidal electromagnetic torque acting at rational surface 1 is given by

$$\delta T_{\phi \mathrm{EM}}(r_1) = \frac{2n\pi^2 R_0}{\mu_0} \left(\frac{\omega_1^+ \tau_1}{(\omega_1^+ \tau_1)^2 + (-E_{11}^+)^2} |C_1^+|^2 \right.$$

$$\left. + \frac{\omega_1^- \tau_1}{(\omega_1^- \tau_1)^2 + (-E_{11}^-)^2} |C_1^-|^2 \right), \tag{13}$$

where use has been made of Eqs. (9), (12), and (A12). This torque modifies the bulk toroidal rotation.[9,12,19] (It is assumed that any modifications to the bulk poloidal rotation are prevented by strong poloidal flow damping.) The steady-state shift induced in the plasma toroidal angular rotation velocity is[9,19]

$$\Omega_\phi(r) = \Omega_\phi(r_1)$$

$$\times \begin{cases} 1, & r < r_1, \\ \displaystyle\int_r^a \frac{dr}{r\mu_\perp(r)} \Big/ \int_{r_1}^a \frac{dr}{r\mu_\perp(r)}, & r_1 \leqslant r \leqslant a, \end{cases}$$

(14)

where a is the minor radius of the outermost plasma flux surface. Here, it is assumed that the toroidal rotation is "clamped" at the edge ($r = a$), so that $\Omega_\phi(a) = 0$.[5,9] The viscous restoring torque that develops at the rational surface is given by[9,19]

$$\delta T_{\phi VS}(r_1) = 4\pi^2 R_0 \times \left[(r\mu_\perp R_0^2) \frac{d\Omega_\phi}{dr} \right]_{r_{1-}}^{r_{1+}}$$

$$= -4\pi^2 R_0 \times \Omega_\phi(r_1) R_0^2 \times \Big/ \int_{r_1}^a \frac{dr}{r\mu_\perp(r)}. \quad (15)$$

In a steady-state plasma the viscous and electromagnetic torques must balance, so

$$\delta T_{\phi EM}(r_1) + \delta T_{\phi VS}(r_1) = 0. \quad (16)$$

Finally, the changes induced in the plasma toroidal angular velocity profile Doppler shift the various natural frequencies, so that

$$\omega_1^\pm \rightarrow \omega_1^\pm - n\Omega_\phi(r_1), \quad (17)$$

where $\omega_1^\pm$ now denote natural frequencies in the *unperturbed* plasma.

3. Torque balance

The balance of electromagnetic and viscous torques in the plasma yields

$$\frac{1}{4} \frac{y^+(1-f)}{(b^+)^2 + (1-f)^2} - \frac{1}{4} \frac{y^- f}{(b^-)^2 + f^2} = f - f_1, \quad (18)$$

where

$$f = \frac{n\Omega_\phi(r_1) - \omega_1^-}{\omega_1^+ - \omega_1^-}, \quad (19a)$$

$$f_1 = \frac{-\omega_1^-}{\omega_1^+ - \omega_1^-}, \quad (19b)$$

$$b^\pm = \frac{-E_{11}^\pm}{|\omega_1^+ - \omega_1^-|\tau_1}, \quad (19c)$$

$$y^\pm = \frac{|C_1^\pm|^2}{\Lambda^2}, \quad (19d)$$

$$\Lambda^2 = \frac{\mu_0 R_0^2}{2 n^2} (\omega_1^+ - \omega_1^-)^2 \tau_1 \Big/ \int_{r_1}^a \frac{dr}{r\mu_\perp(r)}. \quad (19e)$$

In the physically relevant asymptotic limit $b^\pm \ll 1$,[12] Eq. (18) possesses bifurcated solutions. Bifurcations occur in the y^+-y^- plane when the curve of locus,
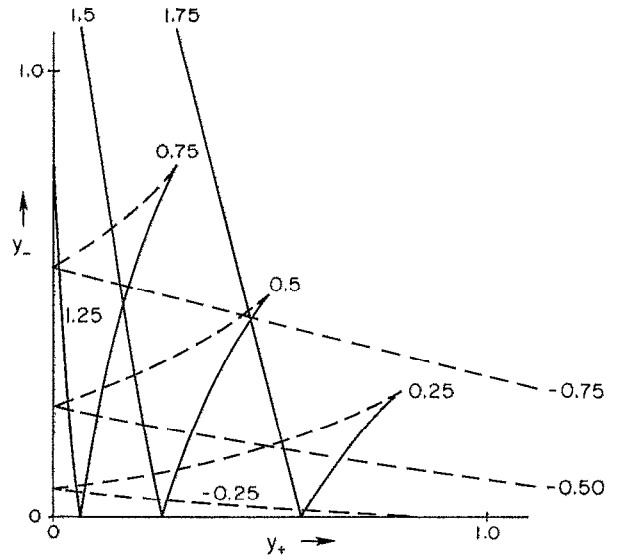

FIG. 1. Bifurcation curves for locking of an external perturbation to the tearing and twisting resonances at a general rational surface. Here y^+ [defined in Eq. (19d)] is the normalized locking torque due to the tearing resonance, and y^- [also defined in Eq. (19d)] is the normalized locking torque due to the twisting resonance. The solid curves correspond to locking to the tearing resonance, whereas the dashed curves correspond to locking to the twisting resonance. Curves are shown for various different values of the unperturbed normalized frequency f_1 [defined in Eq. (19b)].

$$y^+ = 4(2f - f_1)(1 - f)^2,$$
$$y^- = 4(1 - 2f + f_1)f^2, \quad (20)$$

is crossed in the direction of increasing y^+ and y^-. This critical curve is plotted in Fig. 1. The solution can either bifurcate to the tearing resonance at surface 1 ($f = 1$), or the associated twisting resonance ($f = 0$). Prior to bifurcation, there is very little driven tearing or twisting amplitude, whereas after bifurcation, or "*locking*," to the tearing resonance there is substantial driven tearing amplitude at surface 1,

$$\Psi_1^+ \simeq \frac{C_1^+}{(-E_{11}^+)}, \quad (21)$$

and likewise after locking to the twisting resonance there is substantial driven twisting amplitude,

$$\Psi_1^- \simeq \frac{C_1^-}{(-E_{11}^-)}. \quad (22)$$

Locking to either resonance is associated with a sudden change in the steady-state plasma rotation, such as to bring the Doppler shifted natural frequency of the tearing or twisting mode at surface 1 (as appropriate) into coincidence with the applied frequency (which is, of course, zero for a static external perturbation).

Suppose that $|C_1^+|^2 \gg |C_1^-|^2$ (i.e., the locking torque exerted at the rational surface due to externally driven tearing amplitude is much greater than that due to driven twisting amplitude). As is described in Sec. V, this is likely to be the case in low-β tokamak plasmas. In this limit, locking to the

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tearing resonance takes place when the Doppler shifted natural frequency for tearing modes is reduced to one-half its original value [i.e., $\omega_1^+ - n\Omega_\phi(r_1) = \frac{1}{2}\omega_1^+$]. This takes place when

$$|C_1^+|^2 \geqslant \Lambda_1^2 \equiv \frac{\mu_0}{2}\frac{R_0^2}{n}(\omega_1^+)^2\tau_1 \Big/ \int_{r_1}^a \frac{dr}{r\mu_\perp(r)}. \quad (23)$$

4. Discussion

It is clear that the tearing and twisting amplitude driven in a stable tokamak plasma by a static external magnetic perturbation is a highly nonlinear function of the perturbation strength. In fact, there is virtually no driven amplitude until the perturbation strength exceeds a critical value (i.e., $|C_1^+|, |C_1^-| \sim \Lambda$), at which point substantial tearing or twisting amplitude is driven in the plasma. Externally driven tearing amplitude at surface 1 leads to the formation of a stationary chain of magnetic islands whose width is proportional to the square root of the amplitude.[20] Externally driven twisting amplitude leads to the formation of a much narrower chain of "skewed" magnetic islands whose width is directly proportional to the amplitude. Thus, locking of the external perturbation to the twisting resonance at surface 1 is likely to cause less degradation of the plasma confinement than locking to the tearing resonance. A threshold effect for externally induced magnetic tearing in tokamaks has been observed experimentally.[1,3,10]

C. Stability of a plasma containing two rational surfaces

1. Introduction

Suppose that there are two rational surfaces in the plasma (labeled 1 and 2, with $r_2 > r_1$). It is assumed that the

basis tearing and twisting modes associated with the two surfaces are all intrinsically stable, so that $E_{11}^\pm < 0$ and $E_{22}^\pm < 0$. In the following, our investigation is limited to tearing parity modes, for the sake of simplicity. In fact, as is discussed in Sec. V, the components of the C^- vector, which drive twisting parity modes in the plasma, are proportional to the plasma pressure, and can, therefore, be neglected in low-β devices.

2. Electromagnetic and viscous torques

In the physically relevant limit, $\omega_j^+\tau_j \gg 1$ (where j is 1 or 2), the tearing amplitudes driven by a general static external perturbation are given by

$$\Psi_j^+ \simeq -i\,\frac{C_j^+}{\omega_j^+\tau_j}, \quad (24)$$

and the localized electromagnetic locking torques exerted at the rational surfaces are written as

$$\delta T_{\phi\mathrm{EM}}(r_j) \simeq \frac{2n\pi^2 R_0}{\mu_0} \times \frac{|C_j^+|^2}{\omega_j^+\tau_j}. \quad (25)$$

The steady-state shift induced in the plasma toroidal angular velocity profile by these torques takes the form

$$\Omega_\phi(r) = \begin{cases} \Omega_\phi(r_1), & r < r_1, \\[2mm] \Omega_\phi(r_2) + [\Omega_\phi(r_1) - \Omega_\phi(r_2)]\int_r^{r_2}\frac{dr}{r\mu_\perp(r)} \Big/ \int_{r_1}^{r_2}\frac{dr}{r\mu_\perp(r)}, & r_1 \leqslant r \leqslant r_2, \\[2mm] \Omega_\phi(r_2)\int_r^a\frac{dr}{r\mu_\perp(r)} \Big/ \int_{r_2}^a\frac{dr}{r\mu_\perp(r)}, & r_2 < r \leqslant a, \end{cases} \quad (26)$$

which implies the following localized viscous torques acting inside the plasma:

$$\delta T_{\phi\mathrm{VS}}(r_1) = -4\pi^2 R_0 \times [\Omega_\phi(r_1)$$
$$-\Omega_\phi(r_2)]R_0^2 \Big/ \int_{r_1}^{r_2}\frac{dr}{r\mu_\perp(r)}, \quad (27a)$$

$$\delta T_{\phi\mathrm{VS}}(r_2) = -\delta T_{\phi\mathrm{VS}}(r_1) - 4\pi^2 R_0$$
$$\times \Omega_\phi(r_2)R_0^2 \Big/ \int_{r_2}^a\frac{dr}{r\mu_\perp(r)}. \quad (27b)$$

As before, the changes induced in the plasma rotation Doppler shift the various natural frequencies, so that

$$\omega_j^+ \rightarrow \omega_j^+ - n\Omega_\phi(r_j). \quad (28)$$

3. Torque balance

After some manipulation, torque balance at the two rational surfaces yields the following pair of coupled quadratic equations:

$$x^2 - \left(1 - \frac{1}{4}\kappa\,\frac{\beta^2}{y}\right)x + \frac{1}{4}\alpha^2 = 0, \quad (29a)$$

$$y^2 - \left(1 - \frac{1}{4}\frac{\lambda}{\kappa}\frac{\alpha^2}{x}\right)y + \frac{1}{4}\beta^2 = 0, \quad (29b)$$

where the variables

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$$x = \frac{\omega_1^+ - n\Omega_\phi(r_1)}{\omega_1^+}, \quad y = \frac{\omega_2^+ - n\Omega_\phi(r_2)}{\omega_2^+}, \quad (30)$$

are the Doppler shifted natural frequencies normalized with respect to their unperturbed values. The components of the external magnetic perturbation are specified by the parameters

$$\alpha = \left| \frac{C_1^+}{\Lambda_1} \right|, \quad \beta = \left| \frac{C_2^+}{\Lambda_2} \right|, \quad (31)$$

where

$$\Lambda_j^2 = \frac{\mu_0}{2} \frac{R_0^2}{n^2} (\omega_j^+)^2 \tau_j \bigg/ \int_{r_j}^a \frac{dr}{r\mu_\perp(r)}. \quad (32)$$

Note that $\alpha = 1$ corresponds to the critical external perturbation strength required for locking to the tearing resonance at surface 1 in the absence of any torque exerted on surface 2, and *vice versa*. The two remaining parameters,

$$\kappa = \omega_2^+/\omega_1^+, \quad (33a)$$

$$\lambda = \int_{r_2}^a \frac{dr}{r\mu_\perp(r)} \bigg/ \int_{r_1}^a \frac{dr}{r\mu_\perp(r)}, \quad (33b)$$

depend on the nature of the unperturbed plasma equilibrium. Note that $0 \leqslant \lambda < 1$, since $r_2 > r_1$ and $\mu_\perp(r) > 0$.

4. Locking at surface 1

According to Eqs. (29), locking to the tearing resonance at the innermost rational surface (i.e., surface 1) occurs when $\alpha \geqslant \alpha_{\text{crit}}$, where

$$\alpha_{\text{crit}} = 1 - \frac{\kappa}{(1 - \frac{1}{2}\lambda)} \left[\frac{1}{2} \left(1 - \frac{1}{2}\frac{\lambda}{\kappa} \right) \right.$$
$$\left. - \frac{1}{2} \sqrt{\left(1 - \frac{1}{2}\frac{\lambda}{\kappa} \right)^2 - \beta^2 \left(1 - \frac{1}{2}\lambda \right)} \right]. \quad (34)$$

The normalized Doppler shifted natural frequencies just prior to locking are given by $x_{\text{crit}} = \frac{1}{2}\alpha_{\text{crit}}$ and

$$y_{\text{crit}} = \frac{1}{2} \left(1 - \frac{1}{2}\frac{\lambda}{\kappa} \right) + \frac{1}{2} \sqrt{\left(1 - \frac{1}{2}\frac{\lambda}{\kappa} \right)^2 - \beta^2 \left(1 - \frac{1}{2}\lambda \right)}. \quad (35)$$

Locking to the tearing resonance at the outermost rational surface (i.e., surface 2) occurs when $\beta > \beta_{\text{crit}}$, where

$$\beta_{\text{crit}} = 1 - \frac{\lambda}{\kappa(1 - \frac{1}{2}\lambda)} \left[\frac{1}{2} \left(1 - \frac{1}{2}\kappa \right) \right.$$
$$\left. - \frac{1}{2} \sqrt{\left(1 - \frac{1}{2}\kappa \right)^2 - \alpha^2 \left(1 - \frac{1}{2}\lambda \right)} \right] \quad (36)$$

and

$$x_{\text{crit}} = \frac{1}{2} \left(1 - \frac{1}{2}\kappa \right) + \frac{1}{2} \sqrt{\left(1 - \frac{1}{2}\kappa \right)^2 - \alpha^2 \left(1 - \frac{1}{2}\lambda \right)}, \quad (37)$$

with $y_{\text{crit}} = \frac{1}{2}\beta_{\text{crit}}$. Finally, simultaneous locking to the tearing resonances at both surfaces occurs when $\alpha = \alpha_0$ and $\beta = \beta_0$, where

$$\alpha_0 = \frac{(1 - \frac{1}{2}\kappa)}{(1 - \frac{1}{4}\lambda)}, \quad \beta_0 = \frac{[1 - \frac{1}{2}(\lambda/\kappa)]}{(1 - \frac{1}{4}\lambda)}. \quad (38)$$

The normalized Doppler shifted natural frequencies just before simultaneous locking are $x_0 = \frac{1}{2}\alpha_0$ and $y_0 = \frac{1}{2}\beta_0$.

Note that if $\beta = 0$ (i.e., if the external perturbation exerts no torque at surface 2) then locking to the tearing resonance at surface 1 occurs when $\alpha = 1$ (i.e., $|C_1^+| = \Lambda_1$), with $x = \frac{1}{2}$ [i.e., $\omega_1 - n\Omega_\phi(r_1) = \frac{1}{2}\omega_1$], which is equivalent to the simple cylindrical result of Sec. III B (neglecting twisting modes). However, if $\beta > 0$, then locking to the tearing resonance at surface 1 occurs when $\alpha < 1$ (i.e., the threshold locking torque at surface 1 is reduced) with $x < \frac{1}{2}$ [i.e., $\omega_1 - n\Omega_\phi(r_1) < \frac{1}{2}\omega_1$]. Similarly, if $\alpha \neq 0$, then both the threshold torque required to lock the tearing resonance at surface 2 and the critical Doppler shifted natural frequency just prior to locking are less than the cylindrical values.

Figures 2(a)–2(e) show the locking thresholds for the tearing resonance calculated from Eqs. (29) for five different values of the parameter κ, which measures the ratio of the unperturbed natural frequencies for tearing parity modes at the two rational surfaces [see Eq. (33a)]. The thresholds are plotted at constant λ in $\alpha^2 - \beta^2$ space. The locus of the point of simultaneous locking of both surfaces is also plotted. The parameter λ is strongly dependent on the relative positions of the two rational surfaces: $\lambda \rightarrow 1$ as the two surfaces approach one another, and $\lambda \rightarrow 0$ as the outermost surface approaches the edge of the plasma [see Eq. (33b)]. The variables α^2 and β^2 are proportional to the locking torques exerted at surfaces 1 and 2, respectively [see Eqs. (25) and (31)]. These torques are normalized with respect to the threshold locking torques for each surface taken in isolation. For example, $\alpha = 1$ corresponds to the threshold torque required for locking to the tearing resonance at surface 1 when no torque is exerted on surface 2. In Figs. 2, locking does not take place in the region of parameter space bounded by the threshold curve, and the lines $\alpha = 0$ and $\beta = 0$. If the threshold curve is crossed (e.g., by increasing the amplitude of the external perturbation) then locking of either surface 1 or 2 occurs. Surface 2 is locked if the threshold curve is crossed on the low-α side of the simultaneous locking curve, whereas surface 1 is locked if the threshold curve is crossed on the high-α side.

It can be seen from Figs. 2 that reducing the parameter κ favors the locking of surface 2. This is not surprising, since reducing κ corresponds to reducing the unperturbed natural frequency of tearing modes at surface 2 with respect to that at surface 1. For $\kappa < \frac{1}{2}$ and $\lambda < 2\kappa$, surface 2 always locks before surface 1. Similarly, for $\kappa > 2$, surface 1 always locks before surface 2. Increasing λ tends to decrease the threshold torques required to induce locking. This is also not surprising, since if $\lambda \approx 0$ (i.e., if surface 2 lies very close to the plasma edge) a velocity change induced at surface 1 has little effect at surface 2 [see Eq. (26)], so the surface 2 locking criterion is virtually unaffected by the presence of surface 1.
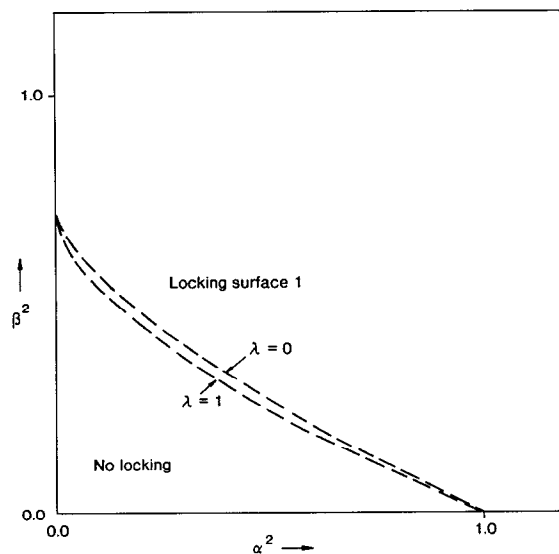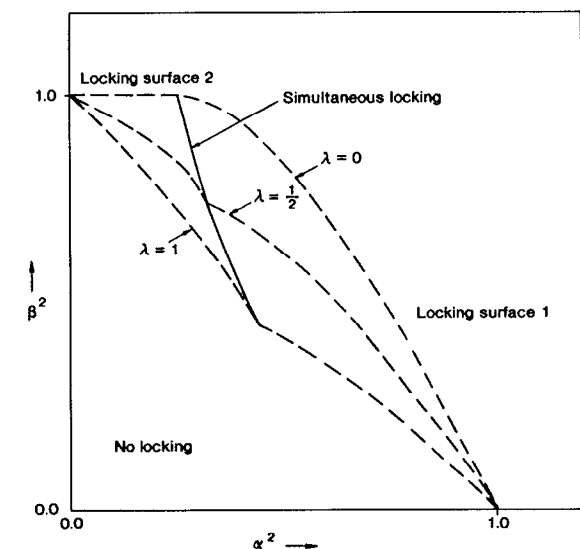
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(a)

(b)

(c)

(d)

(e)
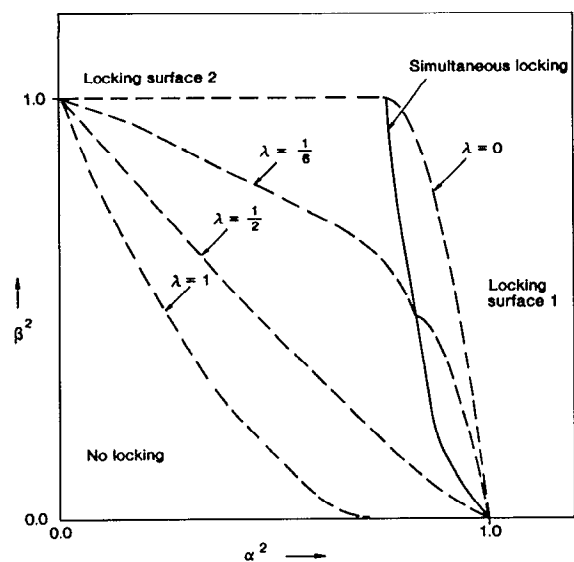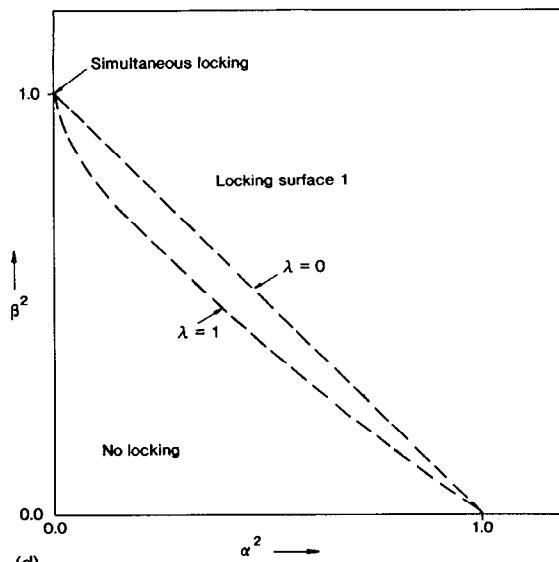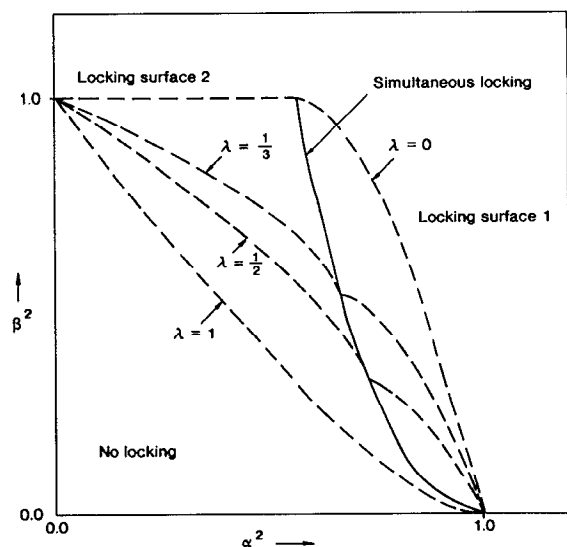
FIG. 2. (a)–(e) Locking thresholds (for the tearing resonances) in a plasma containing two rational surfaces. The variables α^2 and β^2 are proportional to the locking torques exerted at surfaces 1 and 2, respectively. These torques are normalized with respect to the threshold torques for each surface taken in isolation. Curves are plotted for various values of the parameter λ, which depends on the relative positions of the two rational surfaces. The parameter κ measures the ratio of the unperturbed natural frequencies at the two surfaces. (a) shows data for $\kappa=\frac{1}{4}$; (b) shows data for $\kappa=\frac{1}{2}$; (c) shows data for $\kappa=1$; (d) shows data for $\kappa=2$; (e) shows data for $\kappa=4$.

On the other hand, a velocity change induced at surface 2 always has an effect at surface 1, so the locking threshold for surface 1 is reduced somewhat by the presence of surface 2. This type of mutual interaction between the two surfaces is strongest when they are very close together (i.e., when $\lambda \to 1$), so the locking threshold is naturally smallest in this case.

5. Locking at surface 2

Suppose that the tearing resonance at the outermost surface (i.e., surface 2) is locked, so that $n\Omega_\phi(r_2)=\omega_2^+$, but that the innermost surface (i.e., surface 1) remains unlocked. It is easily demonstrated that in the physically relevant limit the tearing amplitude driven at surface 1 satisfies

$$\Psi_1^+ \simeq -i \frac{\tilde{C}_1^+}{[\omega_1^+ - n\Omega_\phi(r_1)]\tau_1}, \tag{39}$$

where

$$\tilde{C}_1^+ = C_1^+ + \frac{E_{12}^+}{(-E_{22}^+)} C_2^+. \tag{40}$$

The usual analysis reveals that locking to the tearing resonance at surface 1 occurs when

$$|\tilde{C}_1^+| \geq \frac{|1-\kappa|}{\sqrt{1-\lambda}} \Lambda_1. \tag{41}$$

If the tearing resonance at surface 1 is locked but surface 2 remains unlocked, then the tearing amplitude driven at surface 2 satisfies

$$\Psi_2^+ \simeq -i \frac{\tilde{C}_2^+}{[\omega_2^+ - n\Omega_\phi(r_2)]\tau_2}, \tag{42}$$

where

$$\tilde{C}_2^+ = C_2^+ + [E_{12}^+/(-E_{11}^+)]C_1^+. \tag{43}$$

It is easily demonstrated that in this case, locking to the tearing resonance at surface 2 occurs when

$$|\tilde{C}_2^+| \geq \frac{|1-\lambda/\kappa|}{\sqrt{1-\lambda}} \Lambda_2. \tag{44}$$

6. Discussion

It is clear from the above analysis that the situation with two rational surfaces in the plasma is far more complicated than that with only one surface, even when twisting resonances are neglected. In general, locking to the tearing resonance at a given rational surface is facilitated by the electromagnetic torque exerted at the other surface, so the locking threshold is reduced somewhat below the single surface value. The critical Doppler shifted natural frequency just before locking is also generally less than the single surface value.

D. Stability of a plasma containing three (or more) rational surfaces

Suppose that there are three rational surfaces in the plasma (labeled 1, 2, and 3, with $r_3 > r_2 > r_1$). It is assumed that all the basis plasma modes are intrinsically stable, and the twisting resonances are again neglected.

Application of the previous analysis to this case, in the physically relevant limit $\omega_j^+ \tau_j \gg 1$, yields the following set of coupled quadratic equations, which control locking to the tearing resonances at the three rational surfaces:

$$x^2 - \left(1 - \frac{1}{4}\kappa_{21}\frac{\beta^2}{y} - \frac{1}{4}\kappa_{31}\frac{\gamma^2}{z}\right)x + \frac{1}{4}\alpha^2 = 0, \tag{45a}$$

$$y^2 - \left(1 - \frac{1}{4}\frac{\lambda_{21}}{\kappa_{21}}\frac{\alpha^2}{x} - \frac{1}{4}\kappa_{32}\frac{\gamma^2}{z}\right)y + \frac{1}{4}\beta^2 = 0, \tag{45b}$$

$$z^2 - \left(1 - \frac{1}{4}\frac{\lambda_{31}}{\kappa_{31}}\frac{\alpha^2}{x} - \frac{1}{4}\frac{\lambda_{32}}{\kappa_{32}}\frac{\beta^2}{y}\right)z + \frac{1}{4}\gamma^2 = 0. \tag{45c}$$

The additional variable $z=[\omega_3^+ - n\Omega_\phi(r_3)]/\omega_3^+$ is the normalized Doppler shifted natural frequency at rational surface 3. The parameter $\gamma=|C_3^+/\Lambda_3|$ specifies the locking torque at surface 3: $\gamma=1$ corresponds to the torque needed for locking to the tearing resonance at this surface when no torques are applied at surfaces 1 and 2. Finally, the parameters

$$\kappa_{ij} = \omega_i^+/\omega_j^+, \tag{46a}$$

$$\lambda_{ij} = \int_{r_i}^a \frac{dr}{r\mu_\perp(r)} \bigg/ \int_{r_j}^a \frac{dr}{r\mu_\perp(r)} \tag{46b}$$

depend on the nature of the unperturbed plasma equilibrium.

Equations (45) can be solved in much the same manner as Eqs. (29) to give the locking thresholds for the various rational surfaces. It is also fairly clear how to extend Eqs. (45) to describe the situation where there are an arbitrary number of surfaces in the plasma.

E. Summary

The above analysis is clearly far more complicated than the zero-β, cylindrical analysis of Refs. 9 and 19. There are two main reasons for this. First, at finite β there is a twisting resonance, as well as a tearing resonance, at every rational surface in the plasma, to which the external perturbation can lock (see Sec. III B). Second, the coupling of different poloidal harmonics in toroidal geometry ensures that even a single helicity external perturbation exerts electromagnetic torques simultaneously at more than one rational surface in the plasma (see Secs. III C and III D). In the above, these effects are investigated separately, but the analysis can easily be extended to deal with both effects simultaneously.

IV. CALCULATION OF THE C^+ VECTOR

A. Introduction

The aim of this section is to classify and characterize the C^+ vectors that are likely to occur in experimental situations. It is demonstrated in the Appendix that the C^+ vector is a function of both the plasma equilibrium and the external perturbation, so in Secs. IV B and IV C we describe how these

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are specified in our investigation. In Sec. IV D we describe the C^+ vector associated with a narrow spectrum external perturbation, whereas in Sec. IV E we deal with the C^+ vector from a broad spectrum perturbation.

B. Specification of the plasma equilibrium

Consider an equilibrium in which the locus of the flux surfaces is given by

$$R = R_0 - r\cos\omega - \Delta(r) + E(r)\cos\omega + T(r)\cos 2\omega + \mathcal{O}(\epsilon^2 a), \tag{47}$$

$$Z = r\sin\omega + E(r)\sin\omega + T(r)\sin 2\omega + \mathcal{O}(\epsilon^2 a).$$

Here, (R, ϕ, Z) are standard cylindrical polar coordinates (with Z in the direction of the toroidal symmetry axis), R_0 is the plasma major radius, r is a radius-like flux surface label, ω is the poloidal angle about the magnetic axis ($r=0$), $\Delta(r)$ is the Shafranov shift of flux surfaces, $E(r)$ is the flux surface ellipticity, and $T(r)$ is the flux surface triangularity. The outermost plasma flux surface lies at $r=a$, where a is the plasma minor radius. The ordering assumptions are that $\epsilon \equiv a/R_0 \ll 1$, and $\Delta(a)$, $E(a)$, and $T(a) \sim \mathcal{O}(\epsilon a)$.

The safety factor profile $q(r)$ is assumed to satisfy

$$q(r) = q_a \frac{(r/a)^2}{1-[1-(r/a)^2]^{q_a/q_0}} - q_a \frac{\lambda}{2}\left(\frac{r}{a}\right)^{2\kappa}$$
$$\times\left[1-\left(\frac{r}{a}\right)^2\right], \tag{48}$$

where q_0 is the central safety factor, q_a is the edge safety factor, and k is a positive integer. The $\mathcal{O}(\epsilon^2)$ edge shear parameter λ is chosen so that the plasma current is zero at $r=a$.[13] In the cylindrical limit, Eq. (48) corresponds to an equilibrium toroidal current profile of the form $j(r) = j_0[1-(r/a)^2]^{q_a/q_0-1}$.

The plasma pressure profile is assumed to satisfy

$$p = p_0[1-(r/a)^2]^2. \tag{49}$$

Here, p_0 is the central plasma pressure, which is conveniently parametrized by the (cylindrical) poloidal beta,

$$\beta_p = 4\mu_0\left(\frac{q_a}{\epsilon a B_0}\right)^2 \int_0^a r p(r)\, dr. \tag{50}$$

The adopted ordering scheme requires $\epsilon\beta_p$ to be small compared with unity.

C. Specification of the external magnetic perturbation

A static external magnetic perturbation can be generated via helical windings or saddle coils, but can also arise by accident if the poloidal and toroidal field coils that support the plasma equilibrium are not properly aligned. An accidentally induced magnetic perturbation is usually referred to as an "error field." A general external perturbation (with a given toroidal mode number n) can be completely specified by a set of complex amplitudes, the I_m, which are basically the expansion coefficients of the vacuum magnetic scalar potential interior to the generating coils in the well-behaved (as

$r\to 0$) toroidal ring functions [see Eqs. (A18), (A34), (A39), and (A40)]. The vacuum perturbation within the generating coils can be shown to reduce to

$$(\delta B_r)_{\rm cy} \simeq i\sum_{m\neq 0} \frac{I_m}{a}\left(\frac{r}{a}\right)^{|m|-1} \exp[i(m\theta - n\phi)] \tag{51}$$

in the cylindrical limit [see Eqs. (A4a), (A19), (A21), and (A22)]. Here, θ is a "straight" poloidal angle that is defined to be zero on the *inboard* midplane.[13]

Table I shows the I_m for a typical $n=1$ external perturbation generated by saddle coils. This example field was employed during a series of controlled experiments performed on the COMPASS-D tokamak and was designed to have predominantly $m/n = 2/1$ helicity.[21] Hence, I_2 is the dominant amplitude after I_0 ($m=0$ perturbations do not interact with resistive modes—see Sec. IV E).

Table II shows the I_m for a typical error field. This example field was generated by the Joint European Torus (JET)[22] poloidal field coil set for a standard limiter discharge with $q_a \simeq 3.2$.[10] It exhibits the broad spectrum that is characteristic of an error field. Note that all the even-m amplitudes are approximately 180° out of phase with the odd-m amplitudes, indicating a dipole-like error field source localized close to the outboard midplane ($\theta = \pi$). In fact, it is known that the dominant contribution to the JET error field in this discharge comes from a pair of vertical field coils (usually referred to as P4) located just above and below the outboard midplane.[10]

In the following, we investigate the effect of two idealized $n=1$ static magnetic perturbations (representative of

TABLE I. Relative amplitudes and phases of the I_m for a typical $n=1$ COMPASS-D RMP field generated by external saddle coils, with 1 kA in the saddle bars, $R_0 = 0.56$ m and $a = 0.20$ m. The absolute amplitude of I_2 is 8.6×10^{-5} T m.

m	$|I_m|$	ϕ_m (°)
−1	0.11	180
0	2.52	180
1	0.11	180
2	1.00	0
3	0.34	180
4	0.19	180
5	0.26	0

TABLE II. Relative amplitudes and phases of the I_m for the $n=1$ error field generated by the JET poloidal field coil set for a typical limiter discharge with $q_a \sim 3.2$. Here, the plasma current and toroidal field are in the same direction, there are 39 turns in the P4 coils, $R_0 = 2.96$ m, and $a = 1.0$ m. The absolute amplitude of I_2 is 2.6×10^{-4} T m.

m	$|I_m|$	ϕ_m (°)
−1	0.39	−178.3
0	1.43	+5.0
1	1.29	−179.1
2	1.00	0.0
3	0.65	+178.4
4	0.35	−4.4
5	0.14	+169.0

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those in Tables I and II) on the stability of the 2/1 tearing mode. The first perturbation is supposed to be representative of the type generally used in "resonant magnetic perturbation" (RMP) experiments,[3,21] and has

$$I_2 \neq 0, \quad I_{m \neq 2} = 0. \tag{52}$$

The second perturbation is supposed to represent an error field generated by a source located on the outboard midplane, and has

$$\cdots -I_{-1} = I_0 = -I_1 = I_2 = -I_3 = I_4 = -I_5 \cdots . \tag{53}$$

Note that, since there is nothing special about the stability of the 2/1 tearing mode, the results of our investigation are also relevant to tearing modes of other helicities. However, they cannot be applied to $m = 1$ internal kink modes, which always require special treatment in tokamaks.[17] Such modes are, therefore, specifically excluded from our investigation (i.e., $q_0 > 1$ in all the examples considered) and will be dealt with in a separate publication.

D. Effect of a RMP field

The interaction of tearing modes with an external magnetic perturbation is governed by the C^+ vector [see Eqs. (1)], which is written as

$$\mathbf{C}^+ = \sum_m I_m \mathbf{C}^{m+} \tag{54}$$

[see Eq. (A44)]. If there are N rational surfaces in the plasma, then the $\mathbf{C}^{m+}$ are $1 \times N$ vectors with real components C_j^{m+} (for $j = 1 - N$). The component C_j^{m+} drives the tearing amplitude on surface j [see Eqs. (12)], and also gives rise to a nonlinear electromagnetic torque acting at this surface [see Eq. (13)].

Consider the interaction of a static RMP field satisfying Eq. (52) with the 2/1 tearing mode. The locking torque exerted at the $q = 2$ surface (labeled surface 1 in the following) is parametrized by $|I_2 C_1^{2+}|^2$ [see Eq. (13)]. It is demonstrated in Sec. 5 of the Appendix that C_j^{m+} is the expansion coefficient (in the vacuum region $r > a$) of the free boundary basis tearing mode associated with surface j in the mth well-behaved (as $R \to \infty$) toroidal ring function. This result, which is obtained from a consideration of toroidal angular momentum conservation, is only valid in the absence of a conducting shell.

In the adopted ordering scheme C_1^{2+}, which describes the interaction of a predominantly $m = 2$ external perturbation with a tearing mode of the *same* dominant helicity, is expanded,

$$C_1^{2+} = \lambda^{(0)} + \lambda^{(1)} \epsilon^2 + \lambda^{(2)} \epsilon^2 \beta_p^2 + \lambda^{(3)} \epsilon^2 \beta_p + \lambda^{(4)} E_a^2$$
$$+ \lambda^{(5)} T_a^2 + \mathcal{O}(\epsilon^3), \tag{55}$$

where $\lambda^{(0)}$ is the cylindrical limit, $\lambda^{(1)}$ is a toroidicity correction, $\lambda^{(2)}$ is a pressure correction, $\lambda^{(3)}$ is a correction due to combined toroidal and pressure effects, $\lambda^{(4)}$ is an ellipticity correction, and $\lambda^{(5)}$ is a triangularity correction. Here, $E_a \equiv E(a)$ is the edge ellipticity parameter and $T_a \equiv T(a)$ is the edge triangularity parameter [see Eqs. (47)]. In general, the free boundary basis tearing modes can only be calculated

by solving the full coupled ideal MHD equations (A6) in the outer region. This is achieved for the large aspect ratio, low-β, weakly shaped equilibria described in Sec. IV B using the T7 code.[13]

Figure 3 shows the expansion coefficients of C_1^{2+} evaluated from the T7 code as a function of q_a in the range 2.5–5.2, for $q_0 = 1.01$ and $k = 4$. Figure 4 shows values of C_1^{2+} calculated for an example equilibrium with $\epsilon = 0.15$, $E_a = 0.15$, $T_a = 0.05$, and $\beta_p = 0.0$ or 1.0.

It can be seen from Fig. 3 that the cylindrical part of C_1^{2+} decays slowly as q_a is increased. This is quite understandable, since as the edge-q is increased (at constant central q), the $q = 2$ surface moves deeper inside the plasma, so the interaction with a fixed external perturbation is likely to get progressively weaker due to range effects. The toroidal correction is found to increase the locking torque exerted at $q = 2$ (i.e., increase C_1^{2+}) for $q_a < 3$, but changes discontinuously as the $q = 3$ surface enters the plasma, so that the torque is decreased by toroidicity for $q_a > 3$. The pressure and toroidal/pressure corrections strongly reinforce the locking torque for $q_a < 3$, but become negligible for $q_a > 3$. The ellipticity correction increases the locking torque for $q_a < 4$, but changes discontinuously as the $q = 4$ surface enters the plasma, so that the torque is decreased by ellipticity for $q_a > 4$. Finally, the triangularity correction increases the locking torque at small edge-q (i.e., $q_a \lesssim 2.7$), decreases the torque at moderate and large edge-q, and behaves discontinuously as the $q = 5$ surface enters the plasma.

The presence of an *ideal* mode rational surface (i.e., a surface on which there is no driven tearing or twisting amplitude, due to rotation effects) situated between the $q = 2$ surface and the plasma boundary has the effect of "shielding" the 2/1 tearing mode from the applied RMP field to some extent, so that there is a discontinuity in C_1^{2+} each time such a surface enters the plasma. It can be seen from Fig. 4 that at low β_p this shielding effect is rather weak, since the discontinuous changes of C_1^{2+} at $q_a = 3$, 4, and 5 are nearly invisible. However, at high β_p the shielding of the 2/1 tearing mode by an ideal $q = 3$ surface becomes more appreciable, yielding a significant drop in C_1^{2+} at $q_a = 3$.

Note that a *locked* rational surface has no shielding effect whatsoever. This can be demonstrated by assuming that the $q = 3$ surface is locked (at the tearing resonance) whenever it lies inside the plasma. According to the analysis of Sec. III C 5, in this situation the locking torque exerted at $q = 2$ is parametrized by $|I_2 \tilde{C}_1^{2+}|^2$, where $\tilde{C}_1^{2+} = C_1^{2+}$ for $q_a < 3$ and

$$\tilde{C}_1^{2+} = C_1^{2+} + \frac{E_{12}^+}{(-E_{22}^+)} C_2^{2+}, \tag{56}$$

for $q_a > 3$. Figure 5 shows $\tilde{C}_1^{2+}$ evaluated as a function of q_a for $q_0 = 1.01$, $k = 4$, $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$, with $\beta_p = 0.0$ and 1.0. It can be seen by comparison with Fig. 4 that a locked $q = 3$ surface does not shield the 2/1 tearing mode from the applied RMP field, since there is no discontinuous reduction in $\tilde{C}_1^{2+}$ as the surface enters the plasma.
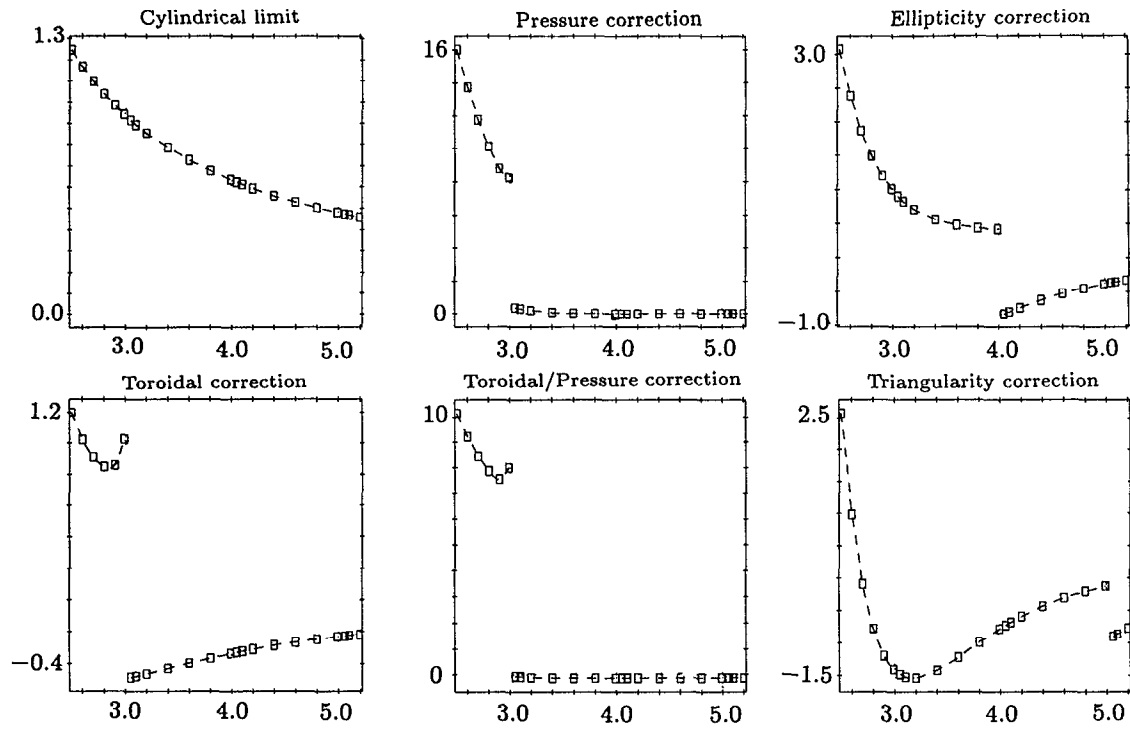
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FIG. 3. The expansion coefficients of C_1^{2+} evaluated as a function of edge q, for $q_0=1.01$ and $k=4$. The various graphs show the cylindrical limit [$\lambda^{(0)}$ in Eq. (55)], the toroidal correction [$\lambda^{(1)}$ in Eq. (55)], the pressure correction [$\lambda^{(2)}$ in Eq. (55)], the toroidal/pressure correction [$\lambda^{(3)}$ in Eq. (55)], the ellipticity correction [$\lambda^{(4)}$ in Eq. (55)], and the triangularity correction [$\lambda^{(5)}$ in Eq. (55)].

E. Effect of an error field

Consider the interaction of an error field satisfying Eq. (53) with the 2/1 tearing mode. The locking torque exerted at the $q=2$ surface is parametrized by $|I_2 C_1^{out+}|^2$, where

$$C_1^{out+} = \cdots - C_1^{-1+} + C_1^{0+} - C_1^{1+} + C_1^{2+} - C_1^{3+} + C_1^{4+}$$
$$- C_1^{5+} + \cdots . \qquad (57)$$

Note that the superscript "out" refers to the outboard location of the coils generating the error field. In the adopted ordering scheme $C_1^{m\neq 2+}$, which governs the interaction of a

tearing mode and an external perturbation with *different* dominant poloidal mode numbers, is expanded,

$$C_1^{m\neq 2+} = \lambda^{(1)}\epsilon + \lambda^{(2)}\epsilon\beta_p + \lambda^{(3)}E_a + \lambda^{(4)}T_a + \mathcal{O}(\epsilon^2). \qquad (58)$$

If the dominant poloidal mode numbers differ by unity, then only $\lambda^{(1)}$ and $\lambda^{(2)}$ are nonzero. If the mode numbers differ by two, or three, then only $\lambda^{(3)}$ or $\lambda^{(4)}$, are nonzero, respectively. If they differ by more than three, then $C_1^{m\neq 2+}$ is negligible.

Figure 6 shows the expansion coefficients of the $C_1^{m\neq 2+}$ calculated from the T7 code as functions of q_a for m in the
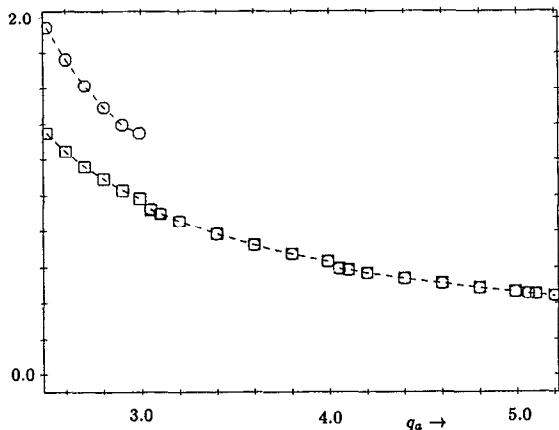

FIG. 4. The parameter C_1^{2+} evaluated as a function of edge q, for $q_0=1.01$ and $k=4$, with $\epsilon=0.15$, $E_a=0.15$, and $T_a=0.05$. Data is shown for $\beta_p=0.0$ ($\square$) and $\beta_p=1.0$ ($\bigcirc$).
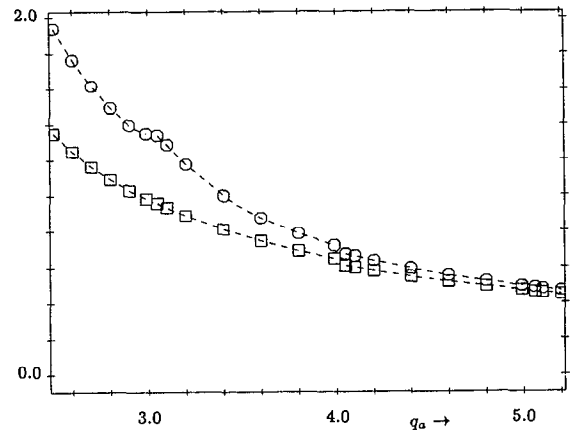

FIG. 5. The parameter $\bar{C}_1^{2+}$ evaluated as a function of edge q, for $q_0=1.01$ and $k=4$, with $\epsilon=0.15$, $E_a=0.15$, and $T_a=0.05$. Data is shown for $\beta_p=0.0$ ($\square$) and $\beta_p=1.0$ ($\bigcirc$).

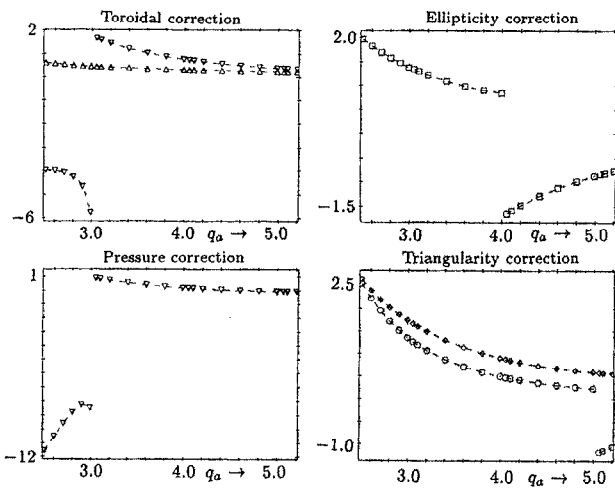R. Fitzpatrick and T. C. Hender   3347

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FIG. 6. Expansion coefficients of the $C_1^{m \neq 2+}$ evaluated as a function of edge q, for $q_0 = 1.01$ and $k = 4$. The various graphs show the toroidal correction [$\lambda^{(1)}$ in Eq. (58)], the pressure correction [$\lambda^{(2)}$ in Eq. (58)], the ellipticity correction [$\lambda^{(3)}$ in Eq. (58)], and the triangularity correction [$\lambda^{(4)}$ in Eq. (58)]. Data is shown for C_1^{-1+} ($\diamond$), C_1^{1+} ($\triangle$), C_1^{3+} (∇), C_1^{4+} ($\square$), and C_1^{5+} ($\bigcirc$).

range -1–5, with $q_0 = 1.01$ and $k = 4$. The expansion coefficients for C_1^{0+} are found to be identically zero (and are, therefore, not plotted), indicating that an $m = 0$ external perturbation does not interact with tearing modes. The quantity C_1^{1+} is found to have no pressure correction. This is due to the peculiar nature of the $m = 1$ harmonic in tokamak plasmas. The expansion coefficients of C_1^{3+} have large discontinuities at $q_a = 3$, showing that the presence of an ideal $q = 3$ surface in the plasma shields the $q = 2$ surface from the influence of a predominantly $m = 3$ external perturbation. The expansion coefficients of C_1^{4+} and C_1^{5+} have similar large discontinuities at $q_a = 4$ and 5, respectively.

Figure 7 shows C_1^{out+} as a function of q_a for $q_0 = 1.01$, $k = 4$, $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$, with $\beta_p = 0.0$ and 0.2. Note the "staircase" variation with edge q, characterized by relatively little change in C_1^{out+} between integer q_a values,
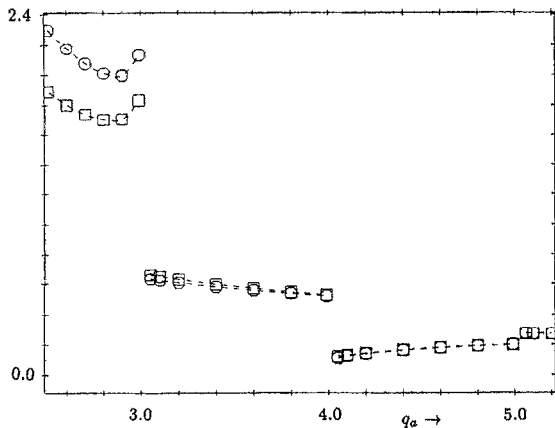

FIG. 7. The parameter C_1^{out+} evaluated as a function of edge q, for $q_0 = 1.01$ and $k = 4$, with $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$. Data is shown for $\beta_p = 0.0$ ($\square$) and $\beta_p = 0.2$ ($\bigcirc$).

with large discontinuities at $q_a = 3$ and 4. The discontinuous reduction in C_1^{1+} at $q_a = 3$ occurs because, as soon as it enters the plasma, an ideal $q = 3$ surface shields the $q = 2$ surface from the $m = 3$ component of the error field. Likewise, the discontinuous reduction at $q_a = 4$ occurs because an ideal $q = 4$ surface shields out the $m = 4$ component of the error field. Note that for a broad spectrum error field the discontinuities are $\mathcal{O}(\epsilon)$, whereas the narrow spectrum RMP field studied in Sec. IV D only yields $\mathcal{O}(\epsilon^2)$ discontinuities. This accounts for the markedly different variations of C_1^{2+} and C_1^{out+} with edge q shown in Figs. 4 and 6, respectively. Note that Fig. 7 would exhibit no discontinuities at $q_a = 3$ and 4 were the $q = 3$ and 4 surfaces locked, since locked surfaces possess no shielding properties (see Sec. IV D).

In experiments, the locking torque exerted at $q = 2$ by a fixed error field is conveniently parametrized by the line-averaged density, below which a static 2/1 island is induced in the plasma. The larger the density, the larger the torque, and vice versa.[4] For narrow spectrum RMP fields, the minimum density is observed to decrease smoothly with increasing edge q,[4] implying a smoothly decreasing locking torque similar to that shown in Fig. 4. On the other hand, for the broad spectrum JET error field (see Table II) the minimum density hardly changes between integer q_a values, but decreases discontinuously as the $q = 3$ and $q = 4$ surfaces enter the plasma.[10] This behavior is consistent with the staircase variation of the locking torque shown in Fig. 7, assuming that both the $q = 3$ and $q = 4$ surfaces are unlocked. Note that discontinuous behavior is only observed in limiter plasmas. For separatrix plasmas, which lie beyond the scope of this paper, there is no observed stepwise variation of minimum density as the ratio of plasma current to toroidal field is changed.[10]

The effect of ideal rational surfaces on the locking torque exerted at $q = 2$ is largely dependent on the relative phases of the different poloidal harmonics of the error field. For an error field source located on the outboard midplane, the phases are such that the torque increases as the $q = 3$ and $q = 4$ surfaces leave the plasma. Consider an error field produced by a source localized on the inboard midplane ($\theta = 0$). For such a field the locking torque exerted at $q = 2$ is parametrized by $|I_2 C_1^{in+}|^2$, where

$$C_1^{in+} = \cdots C_1^{-1+} + C_1^{0+} + C_1^{1+} + C_1^{2+} + C_1^{3+} + C_1^{4+}$$
$$+ C_1^{5+} \cdots . \tag{59}$$

Figure 8 shows C_1^{in+} as a function of q_a for $q_0 = 1.01$, $k = 4$, $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$, with $\beta_p = 0.0$ and 0.2. It can be seen that in this case the phases are such that the locking torque decreases discontinuously as the $q = 3$ surface leaves the plasma, while increasing at $q_a = 4$ and 5. Thus, in this situation the behavior at $q_a = 3$ is opposite to that for the outboard error field source. Even more complicated behavior is obtained if the error field source is located significantly above or below the midplane.

Figure 9 shows C_1^{out+} as a function of q_a for $q_0 = 1.1$, $k = 4$, $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$, with $\beta_p = 0.0$ and 0.2. The increased central-q value brings the plasma very close to the 3/1 ideal external kink stability boundary at $q_a \sim 3$. It can
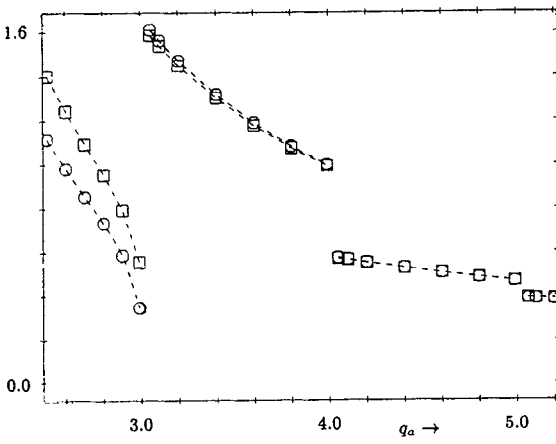
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FIG. 8. The parameter C_1^{in+} evaluated as a function of edge q, for $q_0 = 1.01$ and $k = 4$, with $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$. Data is shown for $\beta_p = 0.0$ ($\square$) and $\beta_p = 0.2$ ($\bigcirc$).

be seen that the torque exerted at $q = 2$ increases very markedly as $q_a \rightarrow 3$ from below. This effect is due to the $m = 3$ component of the error field, as is demonstrated by its sudden disappearance as soon as the $q = 3$ surface, which effectively shields out the $m = 3$ error field, enters the plasma. Figure 9 suggests that the locking torque exerted on the plasma by a fixed error field is likely to become very large close to an ideal external kink stability boundary. This effect may offer an explanation of recent DIII-D results, which imply a substantial increase in the error field locking torque exerted at $q = 2$ as the Troyon β limit is approached.[5]

V. CALCULATION OF THE C^- VECTOR

The interaction of twisting modes with an external perturbation is governed by the C^- vector [see Eqs. (1)], which is written as

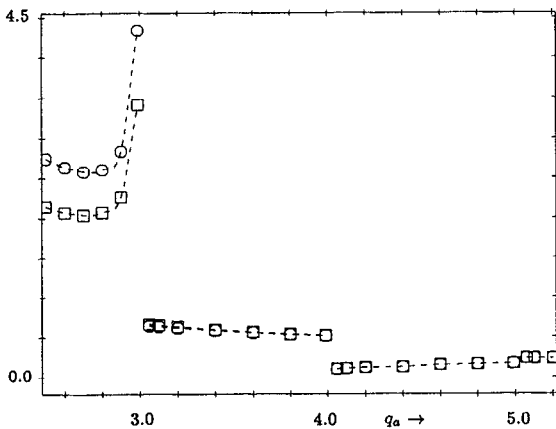$$\mathbf{C}^- = \sum_m I_m \mathbf{C}^{m-} \tag{60}$$

FIG. 9. The parameter C_1^{out+} evaluated as a function of edge q, for $q_0 = 1.1$ and $k = 4$, with $\epsilon = 0.15$, $E_a = 0.15$, and $T_a = 0.05$. Data is shown for $\beta_p = 0.0$ ($\square$) and $\beta_p = 0.2$ ($\bigcirc$).

[see Eq. (A44)]. If there are N rational surfaces in the plasma, then the $\mathbf{C}^{m-}$ are $1 \times N$ vectors with real components C_j^{m-} (for $j = 1 - N$). The component C_j^{m-} drives twisting amplitude on surface j [see Eqs. (12)], and also gives rise to a nonlinear electromagnetic locking torque acting at this surface [see Eq. (13)].

It is demonstrated in Sec. 5 of the Appendix that C_j^{m-} is the expansion coefficient (in the vacuum region $r > a$) of the free boundary basis twisting mode associated with surface j in the mth well-behaved (as $R \rightarrow \infty$) toroidal ring function. As is described in Sec. 4 of the Appendix of Ref. 12, the basis twisting modes can be built up out of solutions of the cylindrical tearing mode equation. Let $\psi_{m_j \pm 1}^L(r)$ be a solution of this equation (for poloidal mode number $m_j \pm 1$) in the interval $0 \leqslant r < r_j$, which satisfies the physical boundary conditions at $r = 0$, is zero at the $m_j \pm 1/n$ rational surface if it lies in the region $0 < r < r_j$, and is unity just inside the m_j/n rational surface at r_{j-}. Likewise, let $\psi_{m_j \pm 1}^R(r)$ be a solution of the cylindrical tearing mode equation in the interval $r > r_j$ that satisfies free boundary conditions for $r > a$, is zero at the $m_j \pm 1/n$ rational surface if it lies in the region $r_j < r \leqslant a$, and is unity just outside the m_j/n rational surface at r_{j+}. It is useful to define the quantities

$$\Delta_{m_j \pm 1}^L = \left(r \frac{d\psi_{m_j \pm 1}^L}{dr} \right)_{r_{j-}},$$

$$\Delta_{m_j \pm 1}^R = \left(r \frac{d\psi_{m_j \pm 1}^R}{dr} \right)_{r_{j+}}. \tag{61}$$

According to Ref. 12, the jth basis twisting mode is built up out of $\mathscr{O}(\epsilon)$ of the $m_j \pm 1$ poloidal harmonics,

$$\psi_{m_j \pm 1}(r) = -\frac{\pi}{2} \frac{\alpha_j}{s_j} (m_j \pm 1)$$

$$\times \left(\frac{\Delta_{m_j \pm 1}^R \pm (m_j \pm 1)(1 + s_j)}{\Delta_{m_j \pm 1}^R - \Delta_{m_j \pm 1}^L} \psi_{m_j \pm 1}^L(r) \right.$$

$$\left. + \frac{\Delta_{m_j \pm 1}^L \pm (m_j \pm 1)(1 + s_j)}{\Delta_{m_j \pm 1}^R - \Delta_{m_j \pm 1}^L} \psi_{m_j \pm 1}^R(r) \right), \tag{62}$$

with only $\mathscr{O}(\epsilon^2)$ of the other poloidal harmonics (including the central m_j harmonic). Here, α_j is the $\mathscr{O}(\epsilon)$ pressure gradient parameter at rational surface j [see Eq. (4)], and $s_j \equiv (rq'/q)_{r_j}$ is the local magnetic shear. It follows from Sec. 5 of the Appendix that

$$C_j^{m_j \pm 1 -} = c_{m_j \pm 1} \alpha_j, \tag{63}$$

where

$$c_{m_j \pm 1} = -\frac{\pi}{s_j} \frac{\Delta_{m_j \pm 1}^L \pm (m_j \pm 1)(1 + s_j)}{\Delta_{m_j \pm 1}^R - \Delta_{m_j \pm 1}^L} \psi_{m_j \pm 1}^R(a), \tag{64}$$

since $\psi_{m_j \pm 1}^L(a) = 0$ by definition [see Eqs. (A27), (A32), (A46), and (A48)]. Note that the C_j^{mk-} are $\mathscr{O}(\epsilon^2)$ for $m_k \neq m_j \pm 1$. Thus, the jth basis twisting mode (resonant with

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TABLE III. Values of λ [defined in Eq. (66)] as a function of q_a, for $q_0 = 1.01$.

q_a	λ
2.5	6.73
2.6	7.14
2.7	7.46
2.8	7.75
2.9	8.27
2.99	9.61

poloidal mode number m_j) is most strongly affected by external perturbations, whose dominant poloidal mode numbers are $m_j \pm 1$.

Consider the interaction of a static RMP field satisfying Eq. (52) with the 2/1 twisting mode. The locking torque exerted at the $q=2$ surface is parametrized by $|I_2 C_1^{2-}|^2$ [see Eq. (13)]. It is clear from the above that $C_1^{2-} \sim \mathcal{O}(\epsilon^2)$, so this torque is $\mathcal{O}(\epsilon^4)$. The locking torque exerted at $q=2$ due to interaction with the 2/1 tearing mode is parametrized by $|I_2 C_1^{2+}|^2$ and is $\mathcal{O}(1)$ (see Sec. IV D). We conclude that in this case the locking torque due to interaction with the 2/1 twisting mode is negligible compared to that associated with the 2/1 tearing mode.

Consider the interaction of an error field satisfying Eq. (53) with the 2/1 twisting mode. The locking torque exerted at the $q=2$ surface is parametrized by $|I_2 C_1^{\text{out}-}|^2$, where

$$C_1^{\text{out}-} = -C_1^{1-} - C_1^{3-} + \mathcal{O}(\epsilon^2). \tag{65}$$

The quantities C_1^{1-} and C_1^{3-} can be evaluated using a cylindrical tearing mode code via Eqs. (63) and (64). It is found that C_1^{1-} is zero (i.e., the 2/1 twisting mode is not affected by a predominantly 1/1 external perturbation). This result is due to the peculiar nature of the $m=1$ harmonic in tokamak plasmas, and is not general. For instance, the 3/1 twisting mode is affected by a predominantly 2/1 external perturbation. It is also found that C_1^{3-} drops discontinuously to zero as the $q=3$ surface enters the plasma, because an ideal $q=3$ surface completely shields the 2/1 twisting mode from the influence of a predominantly 3/1 external perturbation. So, in the adopted ordering scheme,

$$C_1^{\text{out}-} = \lambda \epsilon \beta_p, \tag{66}$$

where λ is zero for $q_a > 3$. Values of λ for q_a in the range 2.5–3.0, and $q_0 = 1.01$, are given in Table III. It is clear that the locking torque due to interaction with the 2/1 twisting mode is zero for $q_a > 3$, and is $\mathcal{O}(\epsilon \beta_p)^2$ for $q_a < 3$. This should be compared with the locking torque due to interaction with the 2/1 tearing mode, which is $\mathcal{O}(1)$, with $\mathcal{O}(\epsilon)$ discontinuities at integer edge q (see Sec. IV E). Thus, if $\epsilon \beta_p \ll 1$, the locking torque associated with the externally driven 2/1 tearing mode again dominates that due to the twisting mode.

VI. SUMMARY

We have examined the influence of a general static external magnetic perturbation on the stability of resistive modes in a tokamak plasma. There are three main parts to this investigation.

First, the vacuum external perturbation must be expanded as a series of well-behaved (as $r \to 0$) toroidal ring functions (see Sec. IV C). A perturbation with a given toroidal mode number is fully specified by the complex coefficients of this expansion, which are denoted by the I_m, where m is the number of poloidal nodes. Typical coefficients for a deliberately applied RMP field and an accidentally occurring error field are given in Tables I and II, respectively. The RMP field considered is designed to have a narrow spectrum with one particular resonant I_m dominant, whereas error fields tend to have broad spectra.

Second, the dispersion relation for resistive modes in the presence of a general external perturbation must be derived (see the Appendix). The unperturbed dispersion relation takes the form of two coupled homogeneous $N \times N$ matrix equations, where N is the number of rational surfaces in the plasma (resonant with a given toroidal mode number). In the presence of an external perturbation these equations acquire right-hand sides, denoted by the $1 \times N$ vectors $\mathbf{C}^\pm$. The C^+ vector characterizes the response of tearing parity modes to the external perturbation, whereas the C^- vector characterizes the response of twisting parity modes. The $C^\pm$ vectors are decomposed, $\mathbf{C}^\pm = \Sigma_m I_m \mathbf{C}^{m\pm}$. It is demonstrated in the Appendix that the components of the $\mathbf{C}^{m\pm}$ vectors are obtainable from the asymptotic behavior (as $R \to \infty$) of the free boundary basis tearing and twisting modes (in the absence of the external perturbation). This result follows from a consideration of toroidal angular momentum conservation, but is only valid in the absence of a conducting shell.

Last, the resistive dispersion relation must be solved to give the tearing and twisting amplitudes driven in the plasma by the external perturbation (see Sec. III). The electromagnetic locking torque exerted at rational surface j is proportional to $|C_j^+|^2$ and $|C_j^-|^2$, where $C_j^\pm$ are the jth components of the $C^\pm$ vectors. Considering the simplest case, where there is only a single rational surface in the plasma and $|C_j^+|^2 \gg |C_j^-|^2$, we find that as soon as $|C_j^+|$ exceeds the critical value needed to *half* the natural frequency for tearing modes at surface j, this frequency suddenly drops to a value very close to zero, and there is a dramatic increase in the driven tearing amplitude. This process is termed "locking." Prior to locking there is very little driven tearing amplitude at surface j.

The problem becomes more complicated if $|C_j^-|^2 \gtrsim |C_j^+|^2$, so that the torque due to driven twisting amplitude at surface j is comparable to that due to the driven tearing amplitude, but this is unlikely to occur in low-β plasmas (see Sec. V). When there is more than one rational surface in the plasma, locking torques are exerted simultaneously at all surfaces, and a change in rotation induced at a given surface can influence the other surfaces via the action of bulk plasma viscosity. We have derived a set of coupled nonlinear equations that describe the response of each rational surface to a general external perturbation (see Sec. III D).

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These equations have been solved for an example case with two rational surfaces in the plasma (see Sec. III C). In general, we find that the critical electromagnetic torque required to lock surface j is reduced if torques are exerted at any other surfaces. Furthermore, locking occurs when the natural frequency of tearing modes at surface j has been reduced to a critical value, which is now somewhat less than half its unperturbed value.

The T7 toroidal tearing mode code[13] has been extended to evaluate the C^{m+} vectors (see Sec. IV). This allows us to construct the C^+ vector, given the complex amplitudes, I_m, which characterize the external perturbation. We have considered two idealized external perturbations. The first has $I_m = I$ with $I_{m' \neq m} = 0$ (where I is a constant) and represents a typical narrow spectrum RMP field produced by external saddle coils. The second has $I_m = (-1)^m I$ and represents an error field produced by a localized source on the outboard midplane.

Consider the locking torque exerted at a typical low mode number rational surface such as $q = 2$. We find that *ideal* rational surfaces located between this surface and the plasma edge tend to "shield" it from the locally resonant component of the applied external perturbation. For instance, an *ideal* 3/1 surface shields out the $m = 3$ component. This effect leads to a discontinuous variation of the locking torque with edge-q. There is a sudden change in the torque as the $q = 3$ surface enters the plasma and shields the $m = 3$ component of the applied perturbation. There is a similar sudden change as the $q = 4$ surface enters the plasma. For a narrow spectrum RMP field, the discontinuous changes in the locking torque at rational edge-q are $\mathcal{O}(\epsilon^2)$ (where ϵ is the inverse aspect ratio), and are not a dominant feature of the variation with edge q. However, for a broad spectrum error field, the discontinuous changes are $\mathcal{O}(\epsilon)$ and tend to be the dominant feature of the edge-q variation. For an error field source located on the outboard midplane, there is a "staircase" variation, with relatively little change between integer edge-q values, but strong reductions at $q = 3$ and 4 (as q_a is increased). Such behavior has been observed experimentally.[10] An error field source located on the inboard midplane, or significantly off the midplane, generally gives rise to a more complicated variation of the locking torque with edge-q (see Fig. 8). We find that *locked* rational surfaces have no shielding effect, so that there is no sudden change in the torque as a locked surface is brought into the plasma. We also find that the locking torque exerted by a fixed error field becomes very large close to an ideal external kink stability boundary. We speculate that this effect may account for the observed significant reduction in the error field strength needed to induce locking at $q = 2$ close to the Troyon β limit in DIII-D.[5]

The components of the C^{m-} vector can be evaluated using solutions of the cylindrical tearing mode equation (see Sec. V). We find that in low-β plasmas, where $\epsilon \beta_p \ll 1$, the locking torques due to externally driven twisting modes are generally negligible compared to the torques associated with driven tearing modes. However, this is unlikely to remain the case in high-β plasmas, where $\epsilon \beta_p \gtrsim \mathcal{O}(1)$.

APPENDIX: PHYSICS OF THE OUTER REGION

1. The marginally stable ideal MHD equations

The coordinate system (r, θ, ϕ), where ϕ is the toroidal angle, θ is an angle-like variable in the poloidal plane, and r is a flux surface label with dimensions of length, is chosen so that the magnetic field lines appear straight. The Jacobian for these coordinates is given by[23]

$$j = (\nabla r \wedge \nabla \theta \cdot \nabla \phi)^{-1} = \frac{rR^2}{R_0}, \tag{A1}$$

where R is the major radius and R_0 is the average major radius of the outermost plasma flux surface. For an axisymmetric equilibrium, the magnetic field $\mathbf{B}$ can be written as

$$\mathbf{B} = B_0 R_0 [f(r) \nabla \phi \wedge \nabla r + g(r) \nabla \phi], \tag{A2}$$

where B_0 is the vacuum magnetic field strength at $R = R_0$. The safety factor, the slope of the field lines in the θ-ϕ plane, is then given by

$$q(r) = \frac{rg(r)}{R_0 f(r)}. \tag{A3}$$

The perturbed magnetic field $\delta \mathbf{B}$ is completely specified by two sets of flux surface functions, $\psi_m(r)$ and $Z_m(r)$, where

$$\delta \mathbf{B} \cdot \nabla r = i \frac{R_0^2}{R^2} \sum_m \frac{\psi_m(r)}{r} \exp[i(m\theta - n\phi)], \tag{A4a}$$

$$R_0 \, \delta \mathbf{B} \cdot \nabla \phi = n \frac{R_0^2}{R^2} \sum_m \frac{[Z_m(r) + \lambda_m \psi_m(r)]}{R_0(m - nq)}$$
$$\times \exp[i(m\theta - n\phi)], \tag{A4b}$$

with

$$\lambda_m = \left(m \frac{\mu_0 r p'}{B_0^2 f^2} \left\langle \frac{R^2}{R_0^2} \frac{1}{|\nabla r|^2} \right\rangle - \frac{m}{n} (m - nq) \frac{R_0 g'}{f} \left\langle \frac{1}{|\nabla r|^2} \right\rangle \right) \Big/ L_m^m,$$

$$L_m^m = \left(m^2 \left\langle \frac{1}{|\nabla r|^2} \right\rangle + n^2 \frac{r^2}{R_0^2} \right), \tag{A5}$$

$$\langle \cdots \rangle \equiv \frac{1}{2\pi} \oint (\cdots) d\theta.$$

Here, the prime denotes differentiation with respect to r, and $p(r)$ is the plasma pressure.

Throughout the bulk of the plasma the perturbed field is governed by the marginally stable equations of ideal magnetohydrodynamics (MHD), which take the form

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$$r \frac{d\psi_m}{dr} = \frac{L_m^m Z_m}{(m-nq)} + \sum_{k \neq 0} \frac{(L_m^{m+k} Z_{m+k} + M_m^{m+k} \psi_{m+k})}{(m+k-nq)},$$

(A6)

$$(m-nq)r \frac{d}{dr}\left(\frac{Z_m}{(m-nq)}\right)$$

$$= \frac{P_m^m \psi_m}{(m-nq)} + \sum_{k \neq 0} \frac{(N_m^{m+k} Z_{m+k} + P_m^{m+k} \psi_{m+k})}{(m+k-nq)}.$$

The coefficients L_m^{m+k}, M_m^{m+k}, N_m^{m+k}, and P_m^{m+k} are evaluated for a general low-β, large aspect ratio tokamak equilibrium in Ref. 13. The ordering adopted is such that the Shafranov shift and departure from circularity of plasma flux surfaces are both $\mathcal{O}(\epsilon)$, with respect to the average minor radius of the outermost plasma flux surface, a, where $\epsilon = a/R_0 \ll 1$ is the inverse aspect ratio. This implies that $L_m^m \sim \mathcal{O}(1) + \mathcal{O}(\epsilon^2)$ and $L_m^{m+k} \sim \mathcal{O}(\epsilon)$, with a similar ordering for the other coefficients. Coupling of harmonics of the perturbed field whose poloidal mode numbers differ by unity is affected by the Shafranov shift of flux surfaces, which is driven by toroidicity and the plasma pressure. Coupling of harmonics whose mode numbers differ by two or three is affected by flux surface ellipticity, or triangularity, respectively. The ordering adopted for the Shafranov shift and flux surface shaping implies that $g = 1 + \mathcal{O}(\epsilon^2)$ and $\mu_0 p/B_0^2 \sim \mathcal{O}(\epsilon^2)$.

2. The outer solution in the vicinity of a rational surface

The marginally stable ideal MHD equations (A6) become singular on flux surfaces where the safety factor q takes the rational value m/n. Such surfaces are termed rational surfaces resonant with poloidal mode number m. The most general expression for the resonant harmonic of the perturbed poloidal flux in the vicinity of a rational surface, radius r_m, is

$$\psi_m \simeq \left[A^+ + \left(\frac{\nu\pi}{2}\right)A^- \text{sgn}(x)\right]|x|^\nu[1+\cdots]$$

$$+ \frac{1}{2}\left[B^+ + \left(\frac{\nu\pi}{2}\right)^{-1}B^- \text{sgn}(x)\right]|x|^{1-\nu} + Cx + \cdots,$$

(A7)

where $x = r - r_m$, and

$$\nu \simeq \left[-\frac{2\mu_0 r p'}{B_0^2 s^2}(1-q^2)\right]_{r_m}$$

(A8)

represents the effect of average field line curvature.[23] Here, $s = (rq'/q)_{r_m}$ is the local magnetic shear, and $A^\pm$, $B^\pm$, and C are arbitrary constants.

The two ratios,

$$\Delta^\pm(\omega) = B^\pm/A^\pm$$

(A9)

are completely determined by the solution of the even and odd parity Fourier transformed layer equations in the inner

region, and are, in general, functions of the mode rotation frequency ω [where all layer quantities are assumed to vary like $\exp(-i\omega t)$].

3. Basis tearing and twisting modes

Suppose there are N rational surfaces in the plasma (radii $r_1 < r_2 \cdots < r_N$), resonant with poloidal mode numbers $m_1, m_2, \ldots, m_N$ (for a fixed toroidal mode number n). It is useful to define the quantities[12]

$$\Psi_j^\pm = \left(\frac{(1-2\nu_j)}{L_{m_j}^{m_j}}\right)^{1/2}_{r_j}(A^\pm)_j,$$

(A10a)

$$\Delta\Psi_j^\pm = \left(\frac{(1-2\nu_j)}{L_{m_j}^{m_j}}\right)^{1/2}_{r_j}(B^\pm)_j,$$

(A10b)

where ν_j is the Mercier index for surface j [see Eq. (A8)], Ψ_j^+ is termed the "tearing amplitude" at surface j, and Ψ_j^- is the associated "twisting amplitude." The tearing amplitude is sometimes referred to as the "reconnected flux." It follows from (A9) that

$$\Delta_j^\pm(\omega) = \frac{\Delta\Psi_j^\pm}{\Psi_j^\pm},$$

(A11)

where $\Delta_j^+(\omega)$ is the tearing parity layer dispersion relation at surface j, and $\Delta_j^-(\omega)$ is the associated twisting parity dispersion relation. The toroidal electromagnetic torque acting in the vicinity of surface j takes the form[12]

$$\delta T_\phi(r_j) = \frac{2n\pi^2 R_0}{\mu_0} \times [\text{Im}(\Delta_j^+)|\Psi_j^+|^2 + \text{Im}(\Delta_j^-)|\Psi_j^-|^2].$$

(A12)

The system has $2N$ degrees of freedom (i.e., two degrees for each rational surface in the plasma), so a general mode can be built up from a linear superposition of $2N$ independent basis modes. It is convenient to define N basis tearing modes, denoted ψ_j^+ (for $j = 1-N$). These are solutions of Eqs. (A6) that satisfy the physical boundary conditions at $r = 0$ and $r = a$, and are subject to the additional constraints:[12]

$$\Psi_k^+ = \delta_{kj},$$

$$\Psi_k^- = 0,$$

$$\Delta\Psi_k^+ = E_{kj}^+,$$

(A13)

$$\Delta\Psi_k^- = H_{jk}.$$

Thus, the jth basis tearing mode has a unit tearing amplitude and a zero twisting amplitude at surface j, with a zero tearing or twisting amplitude at any other surface. It is also convenient to define N basis twisting modes, denoted ψ_j^-. These are solutions of Eqs. (A6) that satisfy the physical boundary conditions and are subject to the constraints[12]

$$\Psi_k^+ = 0,$$

$$\Psi_k^- = \delta_{kj},$$

$$\Delta\Psi_k^+ = H_{kj}, \tag{A14}$$

$$\Delta\Psi_k^- = E_{kj}^-.$$

Thus, the jth basis twisting mode has a unit twisting amplitude and a zero tearing amplitude at surface j, with a zero tearing or twisting amplitude at any other surface. Note that the quantities $E_{kj}^\pm$ and H_{kj} must be *real* because the ideal MHD equations (A6) contain no complex coefficients.

A general mode is written as

$$\psi = \sum_{k=1}^N (\Psi_k^+ \psi_k^+ + \Psi_k^- \psi_k^-), \tag{A15}$$

yielding the resistive mode dispersion relation[12]

$$[\Delta^+(\omega) - E^+]\Psi^+ - H\Psi^- = 0,$$
$$[\Delta^-(\omega) - E^-]\Psi^- - H^\dagger\Psi^+ = 0. \tag{A16}$$

In the above, $E^\pm$ is the $N \times N$ real symmetric matrix of the $E_{ij}^\pm$ values, H is the $N \times N$ real matrix of the H_{ij} values and $H^\dagger$ is its transpose, $\Delta^\pm(\omega)$ is the $N \times N$ complex diagonal matrix of the $\Delta_j^\pm(\omega)$ values, and $\Psi^\pm$ is the $1 \times N$ complex vector of the $\Psi_j^\pm$ values. It follows from Eqs. (A12) and (A16) that

$$T_\phi = \sum_{j=1}^N \delta T_\phi(r_j) = 0, \tag{A17}$$

so there is zero net toroidal electromagnetic torque acting on an isolated plasma.

4. The vacuum region

In the vacuum region external to the plasma the perturbed magnetic field is written as

$$\delta B = i \nabla V, \tag{A18}$$

where the scalar magnetic potential V can be expanded as

$$V(r,\theta,\phi) = \sum_m V_m(r)\exp[i(m\theta - n\phi)]. \tag{A19}$$

It follows from Eqs. (A4) that for $r > a$,

$$Z_m(r) = (m - nq)V_m(r), \tag{A20}$$

and

$$\psi_m(r) = \sum_k \left\langle \frac{R^2}{R_0^2} |\nabla r|^2 \exp(ik\theta) \right\rangle r \frac{dV_{m+k}}{dr}(r)$$

$$- \sum_k \left\langle \frac{R^2}{R_0^2} ir \, \nabla r \cdot \nabla \theta \, \exp(ik\theta) \right\rangle$$

$$\times (m+k)V_{m+k}(r). \tag{A21}$$

In vacuum the scalar magnetic potential satisfies Laplace's equation,

$$\nabla^2 V = 0. \tag{A22}$$

It is easily demonstrated that if V^a and V^b are two general solutions of Eq. (A22) with the same toroidal mode number, then

$$\frac{d}{dr} \sum_k [\psi_k^a(r)V_k^b(r) - \psi_k^b(r)V_k^a(r)] = 0, \tag{A23}$$

where the functions $\psi_k^a(r)$ are related to the functions $V_k^a(r)$ via Eq. (A21).

It is convenient to define the general solution vector ψ, and the related vector V, where the components $\psi_k(r)$ of ψ are the harmonics of the perturbed poloidal flux, so that $\psi(r,\theta,\phi) = \sum_k \psi_k(r)\exp[i(k\theta - n\phi)]$. Likewise, the components $V_k(r)$ of V are the harmonics of the scalar potential, so that $V(r,\theta,\phi) = \sum_k V_k(r)\exp[i(k\theta - n\phi)]$. The components of ψ and V are interrelated via Eq. (A21). Let

$$[\psi^a, \psi^b](r) \equiv \sum_k [\psi_k^a(r)V_k^b(r) - \psi_k^b(r)V_k^a(r)], \tag{A24}$$

where ψ^a and ψ^b are two general solution vectors. It follows from Eq. (A23) that $[\psi^a, \psi^b](r)$ is independent of r in the vacuum region.

In the absence of plasma, the vacuum region extends to the magnetic axis ($r = 0$). In the region close to the axis,

$$\psi_m \simeq r \frac{dV_m}{dr}, \tag{A25}$$

and Laplace's equation reduces to

$$\frac{1}{r}\frac{d}{dr}\left(r \frac{dV_m}{dr}\right) - \frac{m^2}{r^2} V_m \simeq 0, \tag{A26}$$

with solutions $V_m(r) \propto r^{\pm|m|}$ for $m \neq 0$ and $V_0(r) \propto \ln r, r^0$. Let the vacuum basis solution P^m have components that satisfy (A25) and (A26), and reduce to

$$\psi_m(r) = \left(\frac{r}{a}\right)^{-|m|}, \quad \psi_{l \neq m}(r) = 0, \tag{A27}$$

in the limit $r \to 0$. For the special case $m = 0$, the components of the basis solution P^0 reduce to

$$\psi_0(r) = 1, \quad \psi_{l \neq 0}(r) = 0 \tag{A28}$$

at the magnetic axis. Likewise, let the vacuum basis solution Q^m have components that satisfy (A25) and (A26), and reduce to

$$\psi_m(r) = \left(\frac{r}{a}\right)^{+|m|}, \quad \psi_{l \neq m}(r) = 0 \tag{A29}$$

in the limit $r \to 0$. For the special case $m = 0$, the harmonics of the scalar potential derived from the elements of Q^0 [via Eq. (A25)] reduce to

$$V_0(r) = 1, \quad V_{l \neq 0}(r) = 0 \tag{A30}$$

at the magnetic axis. Note that only the Q^m basis solutions are well behaved in the limit $r \to 0$.

It follows from Eqs. (A23), (A24), and (A27)–(A30), that

$$[P^m, P^l](r) = 0, \tag{A31a}$$

$$[Q^m, Q^l](r) = 0, \tag{A31b}$$

$$[\mathbf{P}^m,\mathbf{Q}^l](r)=\delta^{ml}h_m \tag{A31c}$$

throughout the vacuum region, where

$$h_m=\begin{cases}1, & \text{for } m=0,\\ 2/|m|, & \text{for } |m|>0.\end{cases} \tag{A32}$$

The scalar magnetic potential associated with the vacuum basis solution $\mathbf{P}^m$ takes the form[13]

$$V(\mu,\eta,\phi)=\frac{h_m\Gamma(|m|/2-n/2+\tfrac14)\Gamma(|m|/2-n/2+\tfrac34)}{(-1)2^{n+1}(|m|-1)!(-\epsilon)^{-|m|}}$$
$$\times\sqrt{\cosh\mu-\cos\eta}\;P^n_{m-1/2}(\cosh\mu)$$
$$\times\exp[i(m\eta-n\phi)], \tag{A33}$$

and the potential associated with the basis solution $\mathbf{Q}^m$ is written as

$$V(\mu,\eta,\phi)=\frac{2^{|m|+1/2}(|m|-1)!}{(-1)^n\sqrt{\pi}\Gamma(|m|+n+\tfrac12)(-\epsilon)^{|m|}}$$
$$\times\sqrt{\cosh\mu-\cos\eta}\;Q^n_{m-1/2}(\cosh\mu)$$
$$\times\exp[i(m\eta-n\phi)]. \tag{A34}$$

Here, (μ,η,ϕ) are standard toroidal coordinates,

$$R=R_0\,\frac{\sinh\mu}{\cosh\mu-\cos\eta}, \tag{A35a}$$

$$Z=R_0\,\frac{\sin\eta}{\cosh\mu-\cos\eta}, \tag{A35b}$$

while P^b_a and Q^b_a are associated Legendre functions, and $k!=1$ for $k\le0$. Note that only the $\mathbf{P}^m$ basis solutions are well behaved as $R\to\infty$.

The most general solution of the ideal MHD equations in the vacuum region ($r>a$) is written as

$$\psi=\sum_m(a_m\mathbf{P}^m+b_m\mathbf{Q}^m), \tag{A36}$$

where a_m and b_m are arbitrary complex constants. A particular vacuum solution ψ can be resolved into components of the basis solutions $\mathbf{P}^m$ and $\mathbf{Q}^m$ via [see Eqs. (A31)]

$$a_m=h_m^{-1}[\psi,\mathbf{Q}^m](r>a),$$
$$b_m=-h_m^{-1}[\psi,\mathbf{P}^m](r>a). \tag{A37}$$

Finally, it can be demonstrated that the total toroidal electromagnetic torque acting on the plasma satisfies[13]

$$T_\phi(r>a)\equiv\int_0^a\oint\oint R^2\,\nabla\phi\cdot\delta\mathbf{J}\wedge\delta\mathbf{B}\;j\;dr\;d\theta\;d\phi$$
$$=\frac{2n\pi^2R_0}{\mu_0}\times\sum_m h_m\,\mathrm{Im}(a_m^*b_m), \tag{A38}$$

where $\delta\mathbf{J}$ is the perturbed current.

5. The effect of an external helical magnetic field

Consider the effect of a nonrotating externally imposed helical magnetic field on the resistive dispersion relation for a *free boundary* plasma.

The most general solution in the absence of plasma is written as

$$\psi^{\mathrm{vac}}(r<r_{\mathrm{coil}})=\sum_m I_m\mathbf{Q}^m(r), \tag{A39}$$

where the I_m are arbitrary complex constants, and r_{coil} is the innermost radius of the external conductors used to generate the applied field. The scalar magnetic potential of the imposed field in the absence of plasma, V^{ext}, is easily calculated from the currents flowing in these conductors. The corresponding values of the I_m are given by [see Eq. (A34)]

$$I_m=\frac{(-1)^n\sqrt{\pi}\Gamma(|m|+n+\tfrac12)(-\epsilon)^{|m|}}{2^{|m|+1/2}(|m|-1)!Q^n_{m-1/2}(\cosh\mu)}$$
$$\times\oint\oint\frac{V^{\mathrm{ext}}(\mu,\eta,\phi)\exp[-i(m\eta-n\phi)]}{\sqrt{\cosh\mu-\cos\eta}}\frac{d\eta}{2\pi}\frac{d\phi}{2\pi}, \tag{A40}$$

where the integration is carried out on a toroidal surface, $\mu=\mathrm{const}$ [see Eqs. (A35)], lying inside the external conductors.

The most general solution in the presence of plasma is written as

$$\psi(r<r_{\mathrm{coil}})=\sum_{j=1}^N\left[\Psi_j^+\psi_j^+(r)+\Psi_j^-\psi_j^-(r)\right]$$
$$+\sum_m I_m\chi^m(r). \tag{A41}$$

The solution χ^m has the following properties:

$$\Psi_k^\pm=0, \tag{A42a}$$
$$\Delta\Psi_k^\pm=C_k^{m\pm}, \tag{A42b}$$

for $k=1-N$, and

$$\chi^m(r_{\mathrm{coil}}>r>a)=\sum_k h_k^{-1}\alpha_k^m\mathbf{P}^k(r)+\mathbf{Q}^m(r). \tag{A43}$$

Here, the $C_k^{m\pm}$ and α_k^m are arbitrary real constants. Thus, χ^m specifies the *ideal* response of the plasma to the external field associated with the vacuum basis solution $\mathbf{Q}^m$.

It follows from (A13), (A14), (A41), and (A42) that the general externally driven resistive dispersion relation takes the form

$$[\mathbf{\Delta}^+(\omega)-\mathbf{E}^+]\mathbf{\Psi}^+-\mathbf{H}\mathbf{\Psi}^-=\mathbf{C}^+\equiv\sum_m I_m\mathbf{C}^{m+},$$

$$\tag{A44}$$

$$[\mathbf{\Delta}^-(\omega)-\mathbf{E}^-]\mathbf{\Psi}^--\mathbf{H}^\dagger\mathbf{\Psi}^+=\mathbf{C}^-\equiv\sum_m I_m\mathbf{C}^{m-},$$

where the $\mathbf{C}^{m\pm}$ are the $1\times N$ real vectors of the $C_k^{m\pm}$ values.

Using Eqs. (A12) and (A44), the total toroidal electromagnetic torque acting on the plasma is given by

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$$T_\phi(r>a) = \sum_{j=1}^{N} \delta T_\phi(r_j)$$

$$= \frac{2n\pi^2 R_0}{\mu_0} \sum_{m} \sum_{j=1}^{N} \text{Im}\{I_m[C_j^{m+}(\Psi_j^+)^* $$

$$+ C_j^{m-}(\Psi_j^-)^*]\}. \qquad (A45)$$

Since the basis tearing and twisting solutions, ψ_j^+ and ψ_j^-, are well behaved for $r>a$, their most general expansion in the vacuum region is [see Eq. (A36)]

$$\psi_j^\pm(r>a) = \sum_{m} a_{m,j}^\pm \mathbf{P}^m(r), \qquad (A46)$$

where the $a_{m,j}^\pm$ are real constants. Equations (A38), (A41), (A43), and (A46) yield a second expression for the total toroidal electromagnetic torque acting on the plasma:

$$T_\phi(r>a) = \frac{2n\pi^2 R_0}{\mu_0} \sum_{m} \text{Im}\left(\sum_{j=1}^{N} h_m I_m[a_{m,j}^+(\Psi_j^+)^* \right.$$

$$\left. + a_{m,j}^-(\Psi_j^-)^*] + \sum_{l} \alpha_m^l I_m I_l^* \right). \qquad (A47)$$

The identity of Eqs. (A45) and (A47) for arbitrary $\Psi_j^\pm$ and I_m yields $\alpha_m^l = \alpha_l^m$ and

$$C_j^{m+} = h_m a_{m,j}^+ \equiv [\psi_j^+, \mathbf{Q}^m],$$

$$C_j^{m-} = h_m a_{m,j}^- \equiv [\psi_j^-, \mathbf{Q}^m]. \qquad (A48)$$

6. Summary

A general external helical magnetic perturbation can be resolved into components of the well behaved (as $r \to 0$) vacuum basis solutions $\mathbf{Q}^m$ [see Eq. (A39)], so that it is completely specified by a set of complex amplitudes I_m. The I_m are calculated from the scalar magnetic potential of the vacuum external perturbation using Eq. (A40).

The response of the plasma to an idealized perturbation made up of a unit amount of the vacuum basis solution $\mathbf{Q}^m$ is determined by the vectors $\mathbf{C}^{m\pm}$ [see Eqs. (A44)]. The components of these vectors can be obtained by resolving the free boundary basis tearing and twisting modes in the vacuum region $(r>a)$ into components of the well-behaved (as $R \to \infty$) basis vacuum solutions $\mathbf{P}^m$, according to Eqs. (A48). Thus, the response of the plasma to a general perturbation is determined by the vectors $\mathbf{C}^\pm$ [see Eq. (A44)], whose components are obtained from the coefficients of the expansion of the external perturbation in the $\mathbf{Q}^m$ (with no plasma), and the coefficients of the expansion of the basis plasma modes in the $\mathbf{P}^m$ (for $r>a$, with no external perturbation).

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